

# Wrinkling of thin elastic sheets – Lecture 3: The annulus problem

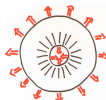
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PCMI, July 2014

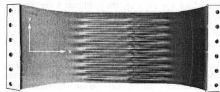
# Today's focus

**Annulus-shaped sheet, loaded by uniform tension** at each boundary.

No wrinkling at larger radii; lots of wrinkling at smaller radii, to avoid compression. Free boundary where wrinkling starts.



Captures essential physics of the “drop on a sheet” (Huang et al, Science 2007) and the “stretched sheet” (Cerdeja & Mahadevan, PRL 2003)



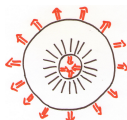
Focus of Davidovitch et al (PNAS 2011) and Bella & Kohn (CPAM 2014).

**Key question:** understand length scale and character of the wrinkling.

**Today's presentation:** “matching” upper & lower bounds on elastic energy. (Arguments provide strong hints but little pointwise information.)

Not discussed today: recent work by Bella (ARMA, in press), providing further insight on behavior near radius where wrinkling stops.

# The big picture



Main result: **excess energy is of order  $h$** . In other words, if

$$E_h = (\text{membrane energy}) + h^2(\text{bending energy}) + (\text{work done by loads})$$

then

$$\mathcal{E}_0 + C_1 h \leq \min E_h \leq \mathcal{E}_0 + C_2 h$$

where  $\mathcal{E}_0$  is the min of the relaxed problem. Really two assertions:

- upper bound (requires a good ansatz, there's a surprise)
- lower bound (ansatz-free, provides interesting intuition)

Recent article with **Peter Bella** (Comm Pure Appl Math 67, 2014, 693-747): fully nonlinear treatment (large strains & rotations, general stress-strain law).

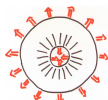
Today's discussion: von Karman version with Poisson's ratio 0 (similar ideas but easier & more transparent).

To be discussed:

- Mathematical formulation
- The relaxed problem
- The lower bound (ansatz-free, provides intuition)
- The upper bound (surprisingly, doesn't match pictures . . .)

sketching the **essential ideas**. Full details available on PCMI site (approx 7 pages).

# Mathematical formulation



$$E_h = (\text{membrane energy}) + h^2(\text{bending energy}) + (\text{work done by loads})$$

$$\text{membrane energy} = \int_{\mathcal{A}} |e(w) + \frac{1}{2} \nabla u_3 \otimes \nabla u_3|^2 dx$$

$$\text{bending energy} = \int_{\mathcal{A}} |\nabla \nabla u_3|^2 dx$$

$$\text{work done by loads} = \int_{|x|=R_{\text{in}}} T_{\text{in}} w \cdot \frac{x}{|x|} ds - \int_{|x|=R_{\text{out}}} T_{\text{out}} w \cdot \frac{x}{|x|} ds$$

where  $\mathcal{A}$  is the annulus. Parameters are  $R_{\text{in}} < R_{\text{out}}$  (geometry),  $T_{\text{in}}$  and  $T_{\text{out}}$  (loads), and  $h$  (thickness).

Some restrictions are needed to make sure the annulus is **wrinkled near  $R_{\text{in}}$**  but **not near  $R_{\text{out}}$** . They turn out to be

$$R_{\text{in}} T_{\text{in}} < R_{\text{out}} T_{\text{out}} \quad \text{and} \quad \frac{T_{\text{in}}}{T_{\text{out}}} > 2 \frac{R_{\text{out}}^2}{R_{\text{in}}^2 + R_{\text{out}}^2}$$

# Polar coordinates

The radial geometry suggests using polar coordinates, not only in space but also for the elastic deformation. Writing  $w_r$  and  $w_\theta$  for the radial and tangential in-plane displacements, we have

$$\text{membrane} = \int_{\mathcal{A}} \left| \begin{array}{c} \partial_r w_r + \frac{1}{2} (\partial_r u_3)^2 \\ * \end{array} r^{-1} (w_r + \partial_\theta w_\theta) + \frac{1}{2} r^{-2} (\partial_\theta u_3)^2 \right|^2 r dr d\theta$$

in which the off-diagonal terms are

$$* = \frac{1}{2} \left( r^{-1} \partial_\theta w_r + \partial_r w_\theta - r^{-1} w_\theta + r^{-1} \partial_r u_3 \partial_\theta u_3 \right);$$

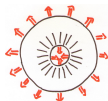
similarly

$$\text{bending} = \int_{\mathcal{A}} (|\partial_{rr} u_3|^2 + 2r^{-2} |\partial_{r\theta} u_3|^2 + r^{-4} |\partial_{\theta\theta} u_3|^2) r dr d\theta$$

and

$$\text{loads} = T_{\text{in}} \int_{r=R_{\text{in}}} w_r r d\theta - T_{\text{out}} \int_{r=R_{\text{out}}} w_r r d\theta.$$

# The relaxed problem



For relaxed problem, we expect “infinitesimal wrinkling” for  $r < L$ , and “biaxial stretching” for  $r > L$ . Sheet has no reason to go out of plane or break radial symmetry. So for relaxed problem,  $u_3 = 0$  and  $w_\theta = 0$ , and  $w_r$  depends only on  $r$ . Recalling from Lecture 2 that

$$\text{relaxed membrane energy} = (e(w) + \frac{1}{2} \nabla u_3 \otimes \nabla u_3)_+^2$$

we see that  $w_r$  minimizes

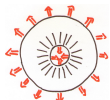
$$\int_{R_{\text{in}}}^{R_{\text{out}}} \left( (\partial_r w_r)_+^2 + (r^{-1} w_r)_+^2 \right) r \, dr + T_{\text{in}} R_{\text{in}} w_r(R_{\text{in}}) - T_{\text{out}} R_{\text{out}} w_r(R_{\text{out}}).$$

We expect  $\partial_r w_r > 0$  (rays should be in tension). Accepting this, the EL eqn (force balance) is

$$\partial_r (r \partial_r w_r) = r^{-1} (w_r)_+$$

with  $2\partial_r w_r(R_{\text{in}}) = T_{\text{in}}$  and  $2\partial_r w_r(R_{\text{out}}) = T_{\text{out}}$ .

# The relaxed problem – cont'd



**The behavior in the wrinkled region is quite explicit:** since prin strains are  $\partial_r w_r > 0$  and  $r^{-1} w_r$ , edge of wrinkled region (call it  $r = L$ ) is where  $w_r = 0$ . Within the wrinkled region, EL eqn becomes  $\partial_r(r\partial_r w_r) = 0$ , so

$$w_r = C \log(r/L) \quad \text{in the wrinkled region.}$$

Notice that

$$\text{compressive strain eliminated by wrinkling} = r^{-1} w_r.$$

**It grows linearly** as  $r$  decreases from  $L$ .



- Mathematical formulation
- The relaxed problem
- The lower bound (ansatz-free, provides intuition)
- The upper bound (surprisingly, doesn't match pictures . . .)

# The lower bound – big picture

**Lower bound** says  $\min E_h \geq \mathcal{E}_0 + Ch$ . Proof must be ansatz-free. Think of  $E_h - \mathcal{E}_0$  as the **excess energy** due to positive  $h$ .

**Step 1:** Soln of  $h = 0$  (“relaxed”) problem is infinitesimally wrinkled but planar. So out-of-plane deformation costs membrane energy. Quantification: if excess energy is less than  $\delta h$ , then (using only membrane effects),

$$\int_{\mathcal{A}} |u_3|^2 \leq C\delta h$$



**Step 2:** The excess energy includes all the bending energy. So if  $u$  has excess energy less than  $\delta h$ , then

$$\int_{\mathcal{A}} |\nabla\nabla u_3|^2 \leq \delta h^{-1}.$$

**Step 3:** Use the interpolation inequality

$$\int_{\mathcal{A}} |\nabla u_3|^2 \leq C_1 \left( \int_{\mathcal{A}} |u_3|^2 \right)^{1/2} \left( \int_{\mathcal{A}} |\nabla\nabla u_3|^2 \right)^{1/2} + C_2 \int_{\mathcal{A}} |u_3|^2$$

to conclude that

$$\int_{\mathcal{A}} |\nabla u_3|^2 \leq C\delta.$$

**Conclusion thus far:** if  $\delta$  is small then the deformation is almost planar.

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**Conclusion thus far:** if  $\delta$  is small then the deformation is almost planar.

# The lower bound – big picture

**Conclusion of Steps 1-3:** if a deformation has excess energy  $E_h - \mathcal{E}_0 \leq \delta h$  then it is almost planar, in the sense that  $\int |\nabla u_3|^2 < C\delta$ .

**Step 4:** For the unrelaxed energy, a deformation that's almost planar has energy that's much too large (greater than  $\mathcal{E}_0$  by an order-one amount).

In fact: small excess energy  $\Rightarrow$  close to relaxed solution. So circles assoc  $r < L$  are shrunk ( $w_r < 0$ ). For unrelaxed energy, compression costs membrane energy.

**So  $\delta$  can't be small**, i.e.  $E_h - \mathcal{E}_0 \geq ch$ . Lower bound is proved.

# The lower bound – more on step 1

In radial coordinates, if  $\tilde{w}_r$  is soln of relaxed problem, then the **excess energy** of  $(w_r, w_\theta, u_3)$  consists of its bending energy (which is positive) plus

$$\int_{\mathcal{A}} \left( \begin{array}{l} \text{unrelaxed membrane} \\ \text{energy of } (w_r, w_\theta, u_3) \end{array} \right) - \int_{\mathcal{A}} \left( \begin{array}{l} \text{relaxed membrane} \\ \text{energy of } (\tilde{w}_r, 0, 0) \end{array} \right) + \left( \begin{array}{l} \text{difference of} \\ \text{loading terms} \end{array} \right)$$

**Claim:** This is equal to

$$\int_{\mathcal{A}} (\partial_r \tilde{w}_r)(\partial_r u_3)^2 + (r^{-1} \tilde{w}_r)_+ (r^{-1} \partial_\theta u_3)^2 + \text{sum of perfect squares.}$$

**The rest is easy:** since  $\partial_r \tilde{w}_r > 0$  (strictly) for all  $r$ , and  $\tilde{w}_r > 0$  (strictly) for  $r > (L + R_{\text{out}})/2$ ,

$$\int_{\mathcal{A}} (\partial_r u_3)^2 + \int_{r > (R_{\text{out}} + L)/2} (\partial_\theta u_3)^2 \leq C \text{ excess energy.}$$

Remembering that  $u_3$  is arbitrary up to a constant (so it should be chosen with mean 0), we get (using a Poincare-type inequality along each ray) that

$$\int_{\mathcal{A}} u_3^2 \leq C \text{ excess energy}$$

as asserted by Step 1.

# About the claim

$$\text{unrelaxed membrane energy of } (w_r, w_\theta, u_3) = \left| \begin{array}{c} \partial_r w_r + \frac{1}{2}(\partial_r u_3)^2 \\ * \\ r^{-1}(w_r + \partial_\theta w_\theta) + \frac{1}{2}(r^{-1}\partial_\theta u_3)^2 \end{array} \right|^2$$

$$\text{relaxed membrane energy of } (\tilde{w}_r, 0, 0) = \left| \begin{array}{cc} \partial_r \tilde{w}_r & 0 \\ 0 & (r^{-1}\tilde{w}_r)_+ \end{array} \right|^2$$

Analogous to our claim, but more familiar: Consider minimizer  $\tilde{\phi}$  of  $\int_\Omega |\nabla \phi|^2 + \int_{\partial\Omega} \phi f$ . For any  $\alpha$  and  $\phi$ , the analogue of our “excess energy” is

$$\text{excess} = \left( \int_\Omega |\nabla \phi + \alpha|^2 + \int_{\partial\Omega} \phi f \right) - \left( \int_\Omega |\nabla \tilde{\phi}|^2 + \int_{\partial\Omega} \tilde{\phi} f \right)$$

To estimate it, observe that

$$\begin{aligned} |\nabla \phi + \alpha|^2 &= |\nabla \tilde{\phi} + \nabla(\phi - \tilde{\phi}) + \alpha|^2 \\ &= |\nabla \tilde{\phi}|^2 + 2\langle \nabla \tilde{\phi}, \nabla(\phi - \tilde{\phi}) \rangle + 2\langle \nabla \tilde{\phi}, \alpha \rangle + |\nabla(\phi - \tilde{\phi}) + \alpha|^2. \end{aligned}$$

Since  $\int_\Omega 2\langle \nabla \tilde{\phi}, \nabla(\phi - \tilde{\phi}) \rangle + \int_{\partial\Omega} (\phi - \tilde{\phi})f = 0$ , we get

$$\text{excess} = \int_\Omega 2\langle \nabla \tilde{\phi}, \alpha \rangle + |\nabla(\phi - \tilde{\phi}) + \alpha|^2$$

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# The upper bound – first pass

**Upper bound** asserts existence of  $(w_r, w_\theta, u_3)$  st  $E_h \leq \mathcal{E}_0 + Ch$ , in other words for which excess energy is of order  $h$ .

**First idea** (unsuccessful!) idea is to wrinkle on scale  $h^{1/2}$ . For such wrinkles the bending term will be of order  $h^2 \cdot (h^{-1/2})^2 \sim h$ . Ansatz:

$$\begin{aligned}w_r &= \tilde{w}_r \\u_3 &= 2\sqrt{2\pi}h^{1/2}(-r\tilde{w}_r)^{1/2} \cos(\theta/h^{1/2}) \quad \text{for } r < L\end{aligned}$$

with  $u_3 = 0$  for  $r > L$ . The tangential displacement  $w_\theta$  should be chosen st

$$r^{-1}w_r + r^{-1}\partial_\theta w_\theta + \frac{1}{2}(r^{-1}\partial_\theta u_3)^2 = 0 \quad \text{pointwise}$$

which is possible since

$$\frac{1}{2} \int_0^{2\pi} (r^{-1}\partial_\theta u_3)^2 d\theta + 2\pi r^{-1}\tilde{w}_r = 0.$$

**This doesn't work:** excess energy is of order  $h|\log h|$ . In fact, ansatz has  $|\partial_r u_3| \sim h^{1/2}|L-r|^{-1/2}$  and

$$\text{excess energy} \geq C \int_{\mathcal{A}} (\partial_r u_3)^2 \geq C \int_{r < L} h|L-r|^{-1} dr$$

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# The upper bound – second pass

A better ansatz uses wrinkling on scale  $\ell(r) \sim h^{1/2}(L-r)^{1/2}$  near  $r = L$ .

**How is this possible?** Wrinkles can refine dyadically. In Euclidean setting, consider wrinkles wrt  $y$ , with  $\int |\partial_y u_3|^2 dy = \frac{1}{2} a^2(x)$ . Refinement from scale  $2\lambda$  at  $x = x_0$  to scale  $\lambda$  at  $x = x_1$  is achieved by taking

$$u_3 = a(x) \left[ f(x) \frac{\lambda}{\pi} \cos\left(\frac{\pi y}{\lambda}\right) + g(x) \frac{\lambda}{2\pi} \cos\left(\frac{2\pi y}{\lambda}\right) \right]$$

with  $f^2 + g^2 = 1$ ,  $f \equiv 1$  for  $x < x_0$ , and  $g \equiv 1$  for  $x > x_1$ . Notice that  $|\partial_x u_3| \sim |a_x| \lambda + a \lambda / (x_1 - x_0)$ . Since change in local scale  $\ell(x)$  satisfies  $\Delta \ell / \Delta x \sim \lambda / (x_1 - x_0)$ , this scheme achieves

$$|\partial_x u_3| \sim |a_x| \ell + a |\ell_x|.$$

Radial case is similar.

**Does it work?** Returning to linear setting, we need  $\int_0^{2\pi} |\partial_\theta u_3|^2 d\theta$  to vanish linearly near  $r = L$ . Use radial analogue of the above, with  $a(r) \sim \sqrt{L-r}$ . Choosing  $\ell \sim h^{1/2} \sqrt{L-r}$  gives  $a(r)|\ell'(r)| + |a'(r)|\ell(r) \sim h^{1/2}$ , so that

$$\text{excess energy} \sim \int_{r \text{ near } L} |\partial_r u_3|^2 \sim h$$

as desired.

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$$u_3 = a(x) \left[ f(x) \frac{\lambda}{\pi} \cos\left(\frac{\pi y}{\lambda}\right) + g(x) \frac{\lambda}{2\pi} \cos\left(\frac{2\pi y}{\lambda}\right) \right]$$

with  $f^2 + g^2 = 1$ ,  $f \equiv 1$  for  $x < x_0$ , and  $g \equiv 1$  for  $x > x_1$ . Notice that  $|\partial_x u_3| \sim |a_x| \lambda + a \lambda / (x_1 - x_0)$ . Since change in local scale  $\ell(x)$  satisfies  $\Delta \ell / \Delta x \sim \lambda / (x_1 - x_0)$ , this scheme achieves

$$|\partial_x u_3| \sim |a_x| \ell + a |\ell_x|.$$

Radial case is similar.

**Does it work?** Returning to linear setting, we need  $\int_0^{2\pi} |\partial_\theta u_3|^2 d\theta$  to vanish linearly near  $r = L$ . Use radial analogue of the above, with  $a(r) \sim \sqrt{L-r}$ . Choosing  $\ell \sim h^{1/2} \sqrt{L-r}$  gives  $a(r)|\ell'(r)| + |a'(r)|\ell(r) \sim h^{1/2}$ , so that

$$\text{excess energy} \sim \int_{r \text{ near } L} |\partial_r u_3|^2 \sim h$$

as desired.

# The upper bound – second pass

A better ansatz uses wrinkling on scale  $\ell(r) \sim h^{1/2}(L-r)^{1/2}$  near  $r = L$ .

**How is this possible?** Wrinkles can refine dyadically. In Euclidean setting, consider wrinkles wrt  $y$ , with  $\int |\partial_y u_3|^2 dy = \frac{1}{2} a^2(x)$ . Refinement from scale  $2\lambda$  at  $x = x_0$  to scale  $\lambda$  at  $x = x_1$  is achieved by taking

$$u_3 = a(x) \left[ f(x) \frac{\lambda}{\pi} \cos\left(\frac{\pi y}{\lambda}\right) + g(x) \frac{\lambda}{2\pi} \cos\left(\frac{2\pi y}{\lambda}\right) \right]$$

with  $f^2 + g^2 = 1$ ,  $f \equiv 1$  for  $x < x_0$ , and  $g \equiv 1$  for  $x > x_1$ . Notice that  $|\partial_x u_3| \sim |a_x| \lambda + a \lambda / (x_1 - x_0)$ . Since change in local scale  $\ell(x)$  satisfies  $\Delta \ell / \Delta x \sim \lambda / (x_1 - x_0)$ , this scheme achieves

$$|\partial_x u_3| \sim |a_x| \ell + a |\ell_x|.$$

Radial case is similar.

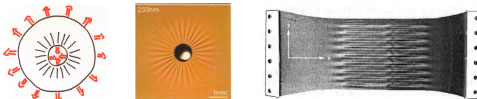
**Does it work?** Returning to linear setting, we need  $\int_0^{2\pi} |\partial_\theta u_3|^2 d\theta$  to vanish linearly near  $r = L$ . Use radial analogue of the above, with  $a(r) \sim \sqrt{L-r}$ . Choosing  $\ell \sim h^{1/2} \sqrt{L-r}$  gives  $a(r)|\ell'(r)| + |a'(r)|\ell(r) \sim h^{1/2}$ , so that

$$\text{excess energy} \sim \int_{r \text{ near } L} |\partial_r u_3|^2 \sim h$$

as desired.

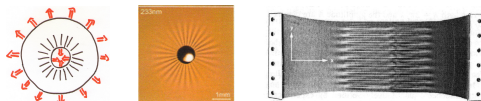


# Stepping back



- The annulus example seems to capture the essential physics of the drop-on-sheet and stretched-sheet experiments.
- Its greater symmetry permits exact soln of relaxed problem.
- Ansatz-free lower bound combines
  - strict convexity of relaxed problem in tensile regime
  - an interpolation inequality (bending term enters here).
- Matching upper bound seems to require refinement of wrinkles.
  - Why do we not see this? Well,  $|\log h|$  is almost a constant.

# Stepping back – cont'd



- Is the minimizer similar to our refinement-of-wrinkles ansatz?
  - Our arguments estimate the energy, but say little about ptwise character of minimizer.
  - Actual behavior near  $r = L$  is probably rather different!
  - For latest progress, see P. Bella, *Transition between planar and wrinkled regions in a uniaxially stretched thin elastic film* (preprint).

Images are from:



E. Cerda and L. Mahadevan, *Phys Rev Lett* 90 (2003) 074302



J. Huang et al, *Science* 317 (2007) 650–653