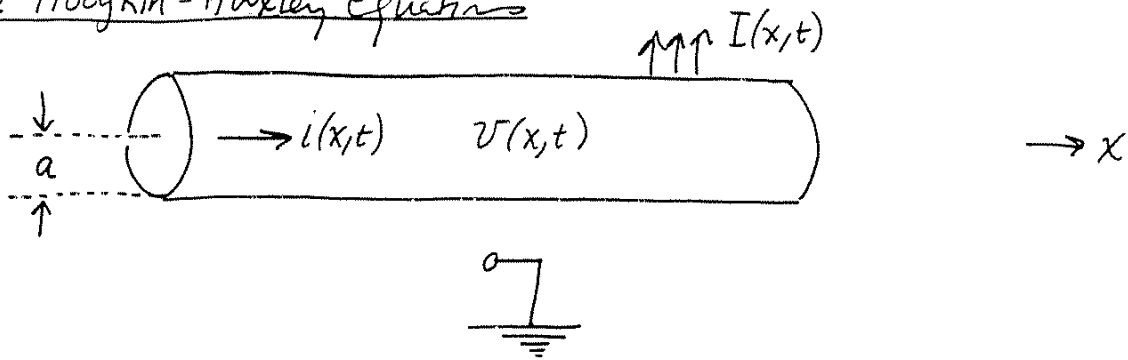


Charles S Peskin 10/11/91

## The Hodgkin-Huxley equations



$a$  = radius of axon

$x$  = distance along axon

$t$  = time

$i(x,t)$  = axial current

$V(x,t)$  = internal voltage

$I(x,t)$  = transmembrane current per unit area

$C$  = membrane capacitance per unit area

$G_{Na}$  =  $Na^+$  conductance per unit area

$G_K$  =  $K^+$  conductance per unit area

$G_L$  = leakage conductance per unit area

$E_{Na}$  = equilibrium potential for  $Na^+$

$E_K$  = equilibrium potential for  $K^+$

$E_L$  = equilibrium potential for leakage current

$\rho$  = resistivity of axoplasm

Current (charge) conservation:

$$i(b,t) - i(a,t) = \int_a^b I(x,t) 2\pi a dx$$

$$\int_a^b \left( \frac{\partial i}{\partial x} + 2\pi a I \right) dx = 0$$

since a and b are arbitrary

$$\frac{\partial i}{\partial x} + 2\pi a I = 0$$

Ohm's law for axial current.

$$i = -\frac{\pi a^2}{\rho} \frac{\partial v}{\partial x}$$

Membrane current is the sum of capacitive and ionic components:

$$I = C \frac{\partial v}{\partial t} + g_{Na}(v - E_{Na}) + g_K(v - E_K) + g_L(v - E_L)$$

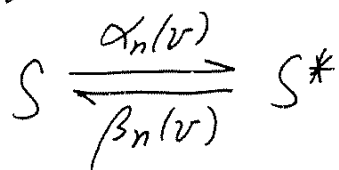
Combining the above:

$$C \frac{\partial v}{\partial t} + g_{Na}(v - E_{Na}) + g_K(v - E_K) + g_L(v - E_L) = \frac{a}{2\rho} \frac{\partial^2 v}{\partial x^2}$$

(This is called the cable equation)

The distinctive feature of the Hodgkin-Huxley equations is the dependence of  $g_K$  and  $g_K$  on voltage and time\*.  
Since it is simpler, consider  $g_K$  first:

Let the  $K^+$  channel consist of 4 identical and independent subunits, each of which has two possible states (S and  $S^*$ ) with voltage dependent transitions.



Let the channel be OPEN if and only if all 4 subunits are in the state  $S^*$ . Now consider a large population of channels, and let  $n$  be the fraction of subunits in the state  $S^*$ . Then  $n^4$  is the fraction of channels in the OPEN state (recall independence of the subunits), and

$$g_K = \bar{g}_K n^4$$

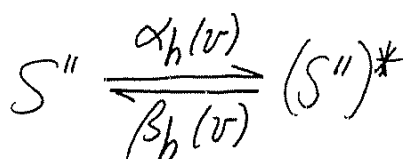
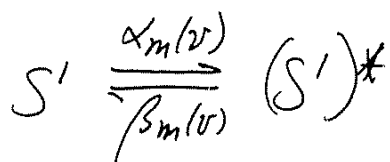
where  $\bar{g}_K$  is the (theoretical)  $K^+$  conductance per unit area that would be achieved if all  $K^+$  channels were open at once. According to the above kinetic scheme,  $n$  satisfies the differential equation

$$\frac{\partial n}{\partial t} = \alpha_n(v)(1-n) - \beta_n(v)n$$

---

\*  $g_L$  is constant:  $g_L = \bar{g}_L$

Now consider  $I_{Na}$ . Let the  $Na^+$  channel also consist of 4 independent subunits, but let 3 be of one type ( $S'$ ) and let 1 be of another type ( $S''$ ). Let each type of subunits have two states with voltage dependent transitions:



and let the channel be open if and only if all 4 subunits are in the state  $*$ :

$$OPEN\ CHANNEL = ((S')^*)_3 (S'')^*$$

In a large population of such channels, let

$$m = \text{fraction of ' subunits in state } (S')^* \\ h = \text{fraction of '' subunits in state } (S'')^*$$

Then  $m^3 h$  is the fraction of OPEN  $Na^+$  channels (recall independence) and

$$I_{Na} = \bar{I}_{Na} m^3 h$$

According to the kinetic schemes given above for  $S'$  and  $S''$ ,  $m$  and  $h$  satisfy the following differential equations

$$\frac{\partial m}{\partial t} = \alpha_m(v)(1-m) - \beta_m(v)m$$

$$\frac{\partial h}{\partial t} = \alpha_h(v)(1-h) - \beta_h(v)h$$

It is often useful to rewrite the equations for  $m, h, n$  as follows:

$$\frac{\partial m}{\partial t} = \frac{1}{\tau_m(v)} (m_{\infty}(v) - m)$$

$$\frac{\partial h}{\partial t} = \frac{1}{\tau_h(v)} (h_{\infty}(v) - h)$$

$$\frac{\partial n}{\partial t} = \frac{1}{\tau_n(v)} (n_{\infty}(v) - n)$$

where

$$m_{\infty}(v) = \frac{\alpha_m(v)}{\alpha_m(v) + \beta_m(v)}$$

$$\tau_m(v) = \frac{1}{\alpha_m(v) + \beta_m(v)}$$

$$h_{\infty}(v) = \frac{\alpha_h(v)}{\alpha_h(v) + \beta_h(v)}$$

$$\tau_h(v) = \frac{1}{\alpha_h(v) + \beta_h(v)}$$

$$n_{\infty}(v) = \frac{\alpha_n(v)}{\alpha_n(v) + \beta_n(v)}$$

$$\tau_n(v) = \frac{1}{\alpha_n(v) + \beta_n(v)}$$

In summary we have the following system:

$$\text{fast} \quad C \frac{\partial v}{\partial t} + \bar{g}_{Na} m^3 h (v - E_{Na}) + \bar{g}_K n^4 (v - E_K) + \bar{g}_L (v - E_L) = \frac{q}{zF} \frac{\partial^2 v}{\partial x^2}$$

$$\text{fast} \quad \frac{\partial m}{\partial t} = \alpha_m(v)(1-m) - \beta_m(v)m = \frac{m_{\infty}(v) - m}{\tau_m(v)}$$

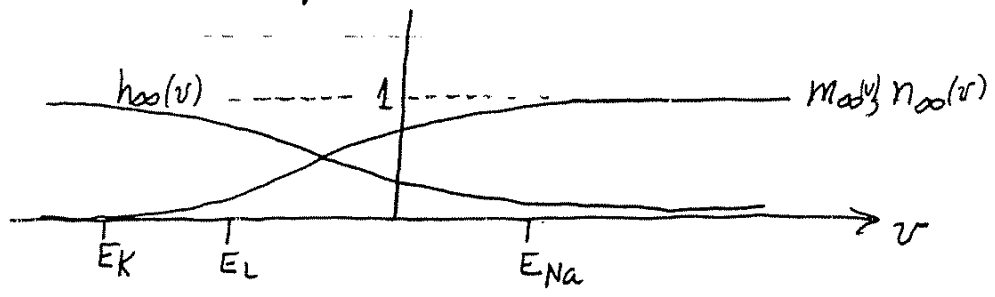
$$\text{slow} \quad \frac{\partial h}{\partial t} = \alpha_h(v)(1-h) - \beta_h(v)h = \frac{h_{\infty}(v) - h}{\tau_h(v)}$$

$$\text{slow} \quad \frac{\partial n}{\partial t} = \alpha_n(v)(1-n) - \beta_n(v)n = \frac{n_{\infty}(v) - n}{\tau_n(v)}$$

The essential qualitative facts which determine the behavior of this system are as follows. First

$$E_K < E_L < 0 < E_{Na}$$

Next,  $m_{\infty}(v)$  and  $n_{\infty}(v)$  are increasing functions, whereas  $h_{\infty}(v)$  is a decreasing function; something like this:



Finally,  $(v, m)$  are fast variables, whereas  $(h, n)$  are slow.

## Qualitative behavior of the "space-clamped" Hodgkin-Huxley equations.

Hodgkin and Huxley worked with the squid giant axon, an axon which is so large that it is possible to insert a silver wire along its length. Since silver is an excellent conductor, this forces  $v(x,t)$  to be independent of  $x$ . Then  $m, h$ , and  $n$  rapidly fall into line with  $v$  and become  $x$ -independent also. (Think about how to show this!) In this space-clamped situation, then, we are dealing with a system of ordinary differential equations. The silver wire can also be used to apply current to the membrane. Thus, the first of the Hodgkin-Huxley equations becomes

$$C \frac{\partial v}{\partial t} + \bar{g}_{Na} m^3 h (v - E_{Na}) + \bar{g}_K n^4 (v - E_K) + \bar{g}_L (v - E_L) = I_0(t)$$

where  $I_0(t)$  is the applied current (per unit area of membrane).

The  $m, h, n$  equations are the same as before. We shall give a qualitative analysis of this system based on the separation into fast and slow time scales.

## Fast time-scale behavior: the $(m, v)$ plane

On a fast time scale ( $\sim 1$  ms),  $h$  and  $n$  are effectively constant, and one can study the behavior of the system in the  $(m, v)$  plane. For now, let  $I_0 = 0$ . The first step is to plot the curves\* along which  $\partial m / \partial t = 0$  or  $\partial v / \partial t = 0$ . The curve  $\partial m / \partial t = 0$  is already known. It is  $m = m_\infty(v)$ . Setting  $\partial v / \partial t = 0$ , we find

$$v = \frac{\bar{g}_{Na} m^3 h E_{Na} + \bar{g}_K n^4 E_K + \bar{g}_L E_L}{\bar{g}_{Na} m^3 h + \bar{g}_K n^4 + \bar{g}_L}$$

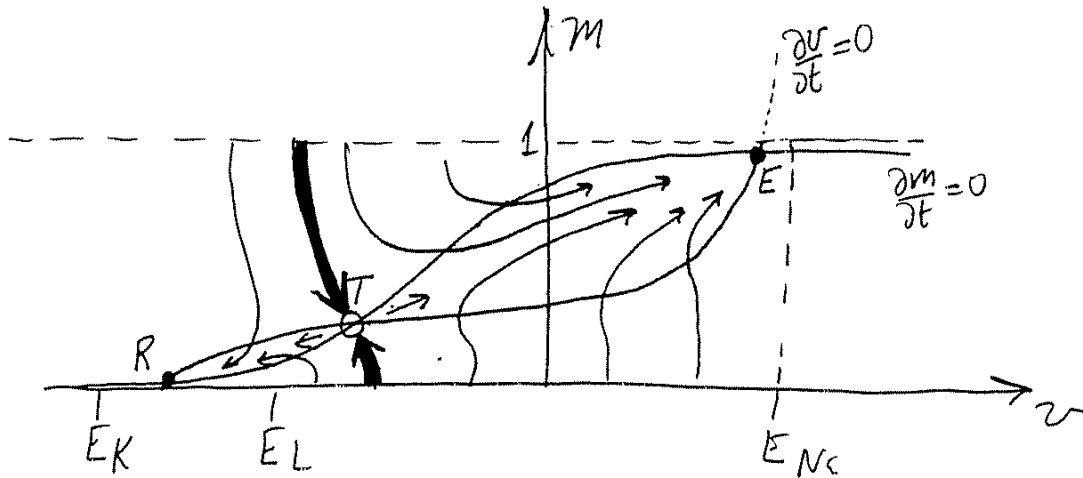
When  $m=0$ ,  $E_K < v < E_L$

As  $m \rightarrow \infty$ ,  $v \rightarrow E_{Na}$  (In fact  $m \leq 1$ , but it helps in sketching the curve to know this limiting value.)

Depending on parameters and on the values of  $h$  and  $n$  (which are treated as parameters in the fast-scale analysis), the curves  $\partial m / \partial t = 0$  and  $\partial v / \partial t = 0$  may have one intersection or three (2 in border-like cases); we consider the situation where the number of intersections is 3.

\* called isoclines





The three intersections have the following character:

R = rest state (stable, node)

T = threshold (unstable, saddle point)

E = excited state (stable, node)

All trajectories that start near R end up at R

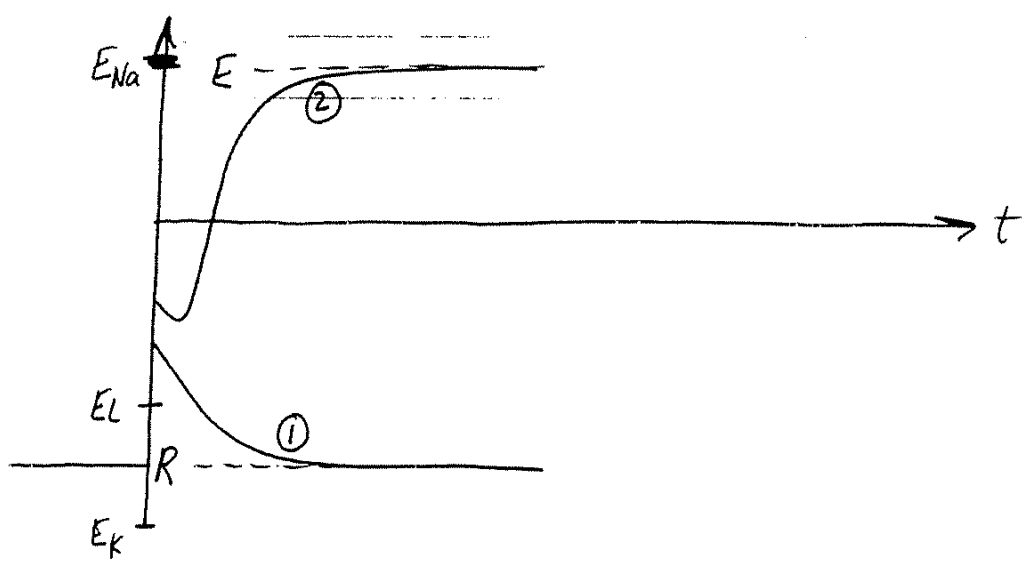
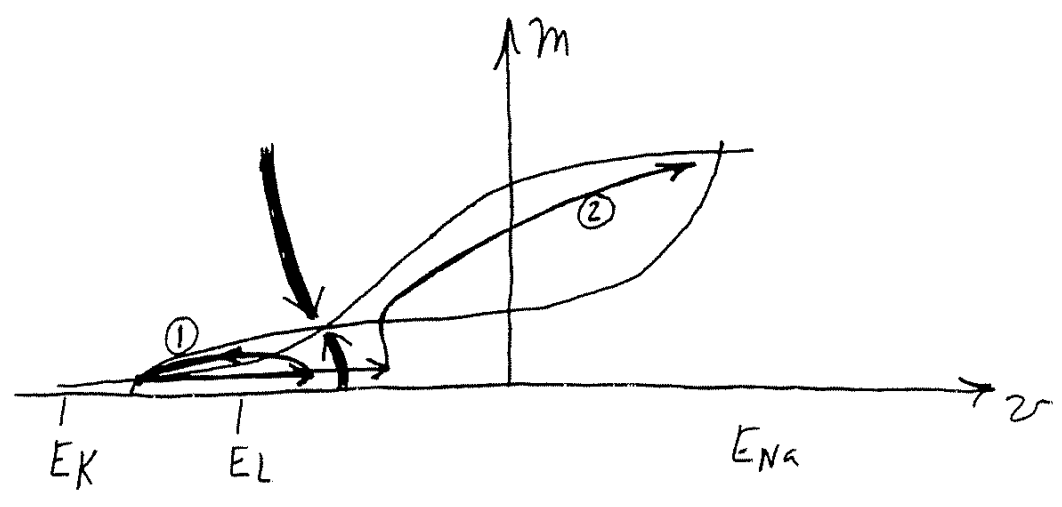
All trajectories that start near E end up at E

At T, there are two special trajectories, drawn dark, that end up at T itself; all others turn away from T and end up at R or E. The special trajectories form a separatrix which divides the phase plane into two parts. Any initial condition to the left of the separatrix has a trajectory that ends at state R; any initial condition to the right has a trajectory that ends at state E.

In summary, the fast-scale behavior is bistable.

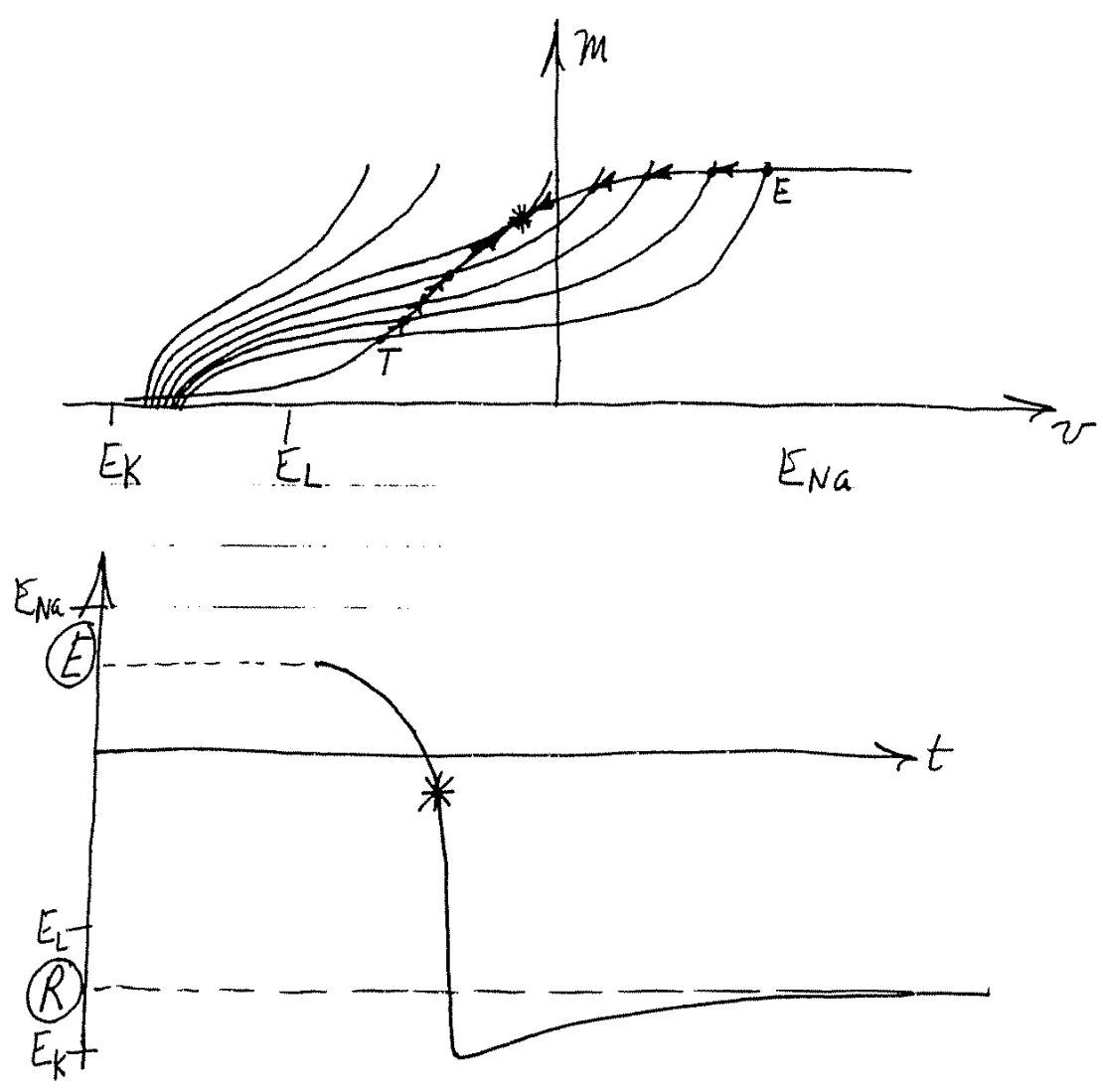
Sub-threshold and supra-threshold excitation :

Let the system be in state R prior to  $t=0$ , and let  $I_0(t) = Q_0 \delta(t)$ , so that  $Q_0$  is the total charge per unit area delivered to the membrane by a current shock applied at  $t=0$ . This produces a jump in voltage  $\Delta V = Q_0/C$ . Since  $m$  cannot change instantaneously, the move in the phase plane is a horizontal shift  $\Delta V$ . If this takes the system past the separatrix, the result is excitation; otherwise, the system returns to rest.



# Recovery following excitation

If  $h$  and  $n$  were really constant, the excited state would persist indefinitely (unless a negative stimulus were applied of sufficient magnitude to cross the separatrix again and return the system to rest.) In fact, however,  $h$  and  $n$  change slowly, and the whole phase portrait evolves in such a way that the states  $E$  and  $T$  collide and mutually annihilate leaving only the state  $R$ , to which the system then returns. This process can be pictured as follows:



## Slow time scale. the $n, v$ plane

We have just been looking at a slow-scale process, in terms of the changes that it makes in the structure of the fast-scale phase plane. A more direct look at the slow time scale can be obtained as follows:

As a preliminary step, we simplify matters by setting

$$h = 1 - n$$

This is consistent with the Hodgkin-Huxley equations if

$$h_{\infty}(v) + n_{\infty}(v) = 1$$

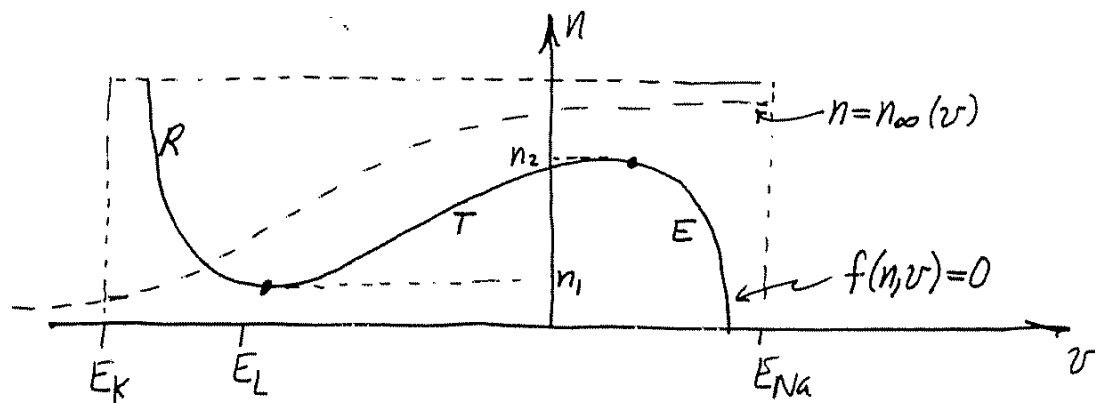
$$\tau_n(v) = \tau_h(v)$$

Next, we come to the essence of the slow-scale analysis, which is to assume that the fast scale variables ( $m, v$ ) are always "at equilibrium" at  $n$  (and hence  $h$ ) evolves. Thus

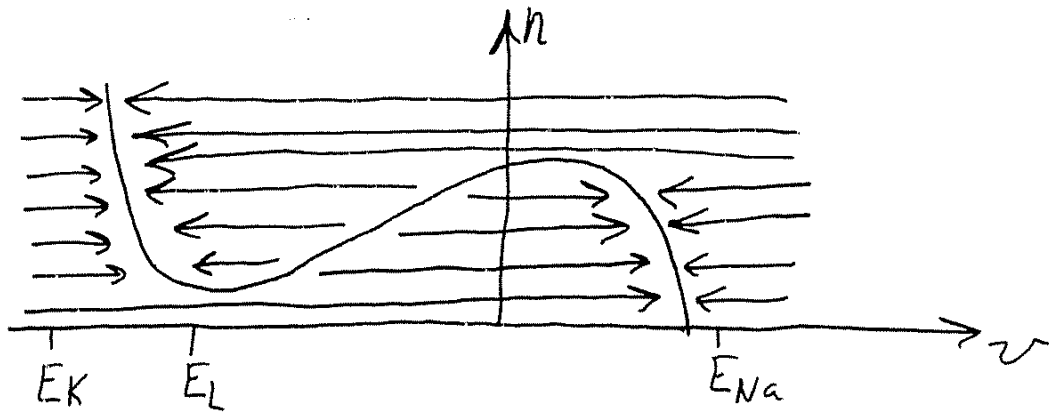
$$m = m_{\infty}(v)$$

$$f(n, v) = \bar{g}_{Na} (m_{\infty}(v))^3 (1-n)(v - E_{Na}) + \bar{g}_K n^4 (v - E_K) + \bar{g}_L (v - E_L) = 0$$

The curve  $f(n,v)=0$  looks like this:



It is called the slow manifold. Note that there is an interval of  $n$ , between  $n_1$  and  $n_2$ , where there are three values of  $v$  corresponding to each value of  $n$ . These correspond to the three constant states  $R, T, E$  of the fast  $(m,v)$  phase plane. Whenever the system is not on the slow manifold, it moves rapidly there by means of changes in the fast variables. On the slow time scale, these rapid changes look like jumps. Since  $n$  doesn't change during these jumps, they appear as horizontal lines in the  $(n,v)$  phase plane. From the fast-scale analysis, we know that the part of the slow manifold labeled  $T$  is unstable. Hence, all trajectories that start off the slow manifold jump horizontally ( $n = \text{constant}$ ) to the branch  $R$  or  $E$  of the slow manifold, as shown below:

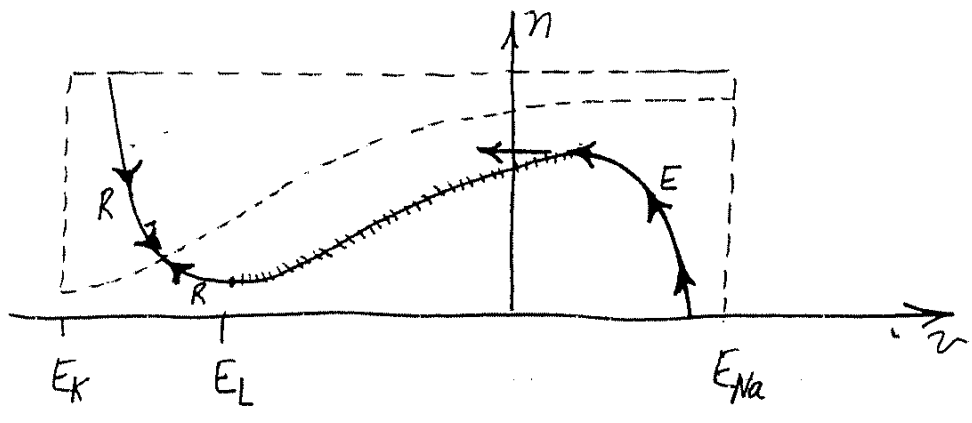


Once it reaches the slow manifold, the system evolves according to

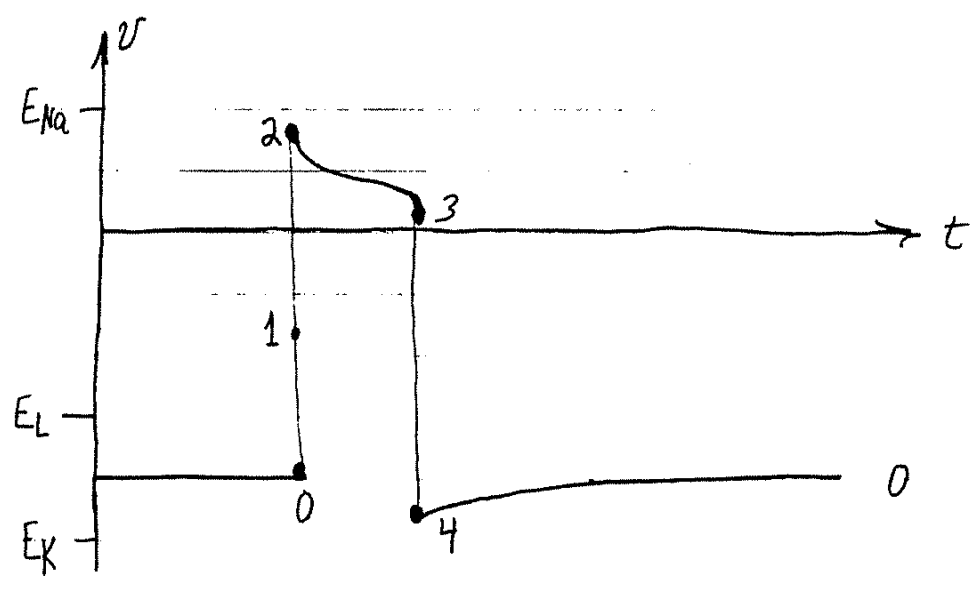
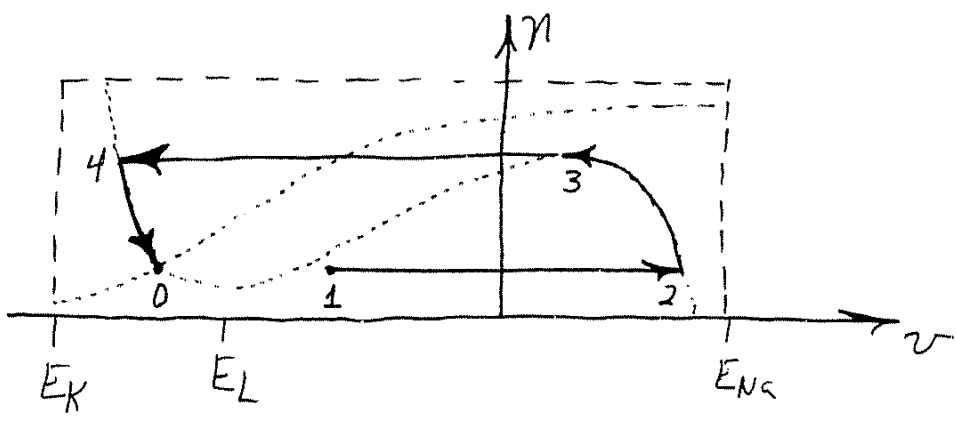
$$\frac{\partial n}{\partial t} = \frac{n_{\infty}(v) - n}{\tau_n(v)}$$

where  $v = v_R(n(t))$  or  $v = v_E(n(t))$  depending on whether the system happens to be on the rest (R) branch or on the excited (E) branch of the slow manifold. ( $v_R(n)$  and  $v_E(n)$  are the two stable solutions of  $f(n, v) = 0$ .  $v_R$  is defined for  $n_1 \leq n \leq 1$  and  $v_E$  is defined for  $0 \leq n \leq n_2$ . Since  $n_1 < n_2$ , their domains overlap.)

The evolution along the slow manifold carries  $n$  towards  $n_{\infty}(v)$ . The curve  $n = n_{\infty}(v)$  intersects the R branch of the slow manifold, but not the E branch. Hence, on the R branch, the  $n$  dynamics carries the system towards a stable resting state, but on the E branch, the  $n$  dynamics drives the system towards and then past the value  $n = n_2$ , where the E branch terminates. The only possibility at that point is to jump to the R branch.



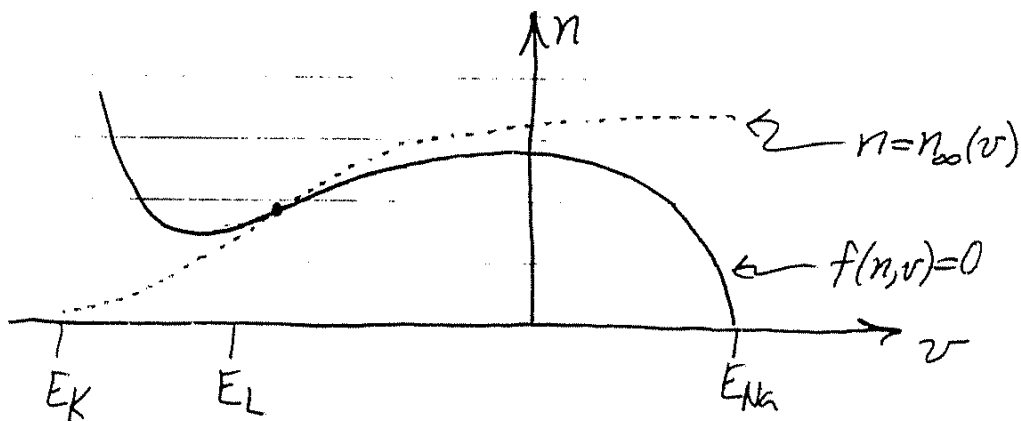
An action potential can now be understood as follows. The rest state of the neuron is the intersection of the curve  $f(n, v) = 0$  (the slow manifold) with the curve  $n = n_{\infty}(v)$ . Let a neuron be at rest there and let a current pulse be applied which is sufficient to step the voltage across the T branch of the slow manifold. Then the neuron jumps to the E manifold, where it evolves to the top, jumps back to the R manifold, and then recovers to its starting point.





Homework: Use the  $(n, v)$  phase plane to discuss the following phenomena. (Don't just answer in words; draw pictures!)

- 1) Relative refractory period: Following an action potential, a second stimulus is given during the recovery phase (between point 4 and the return to point 0 in the diagrams on the previous page). What can you say about (i) the threshold voltage that must be reached to achieve an action potential, (ii) the size of the voltage step required to reach threshold, (iii) the peak voltage achieved during the action potential, (iv) the duration of the action potential.
- 2) Spontaneous oscillations: Suppose the slow manifold is shifted\* so that it intersects the curve  $n = n_{\infty}(v)$  somewhere on the unstable (T) branch of the slow manifold. Then the  $(n, v)$  phase plane looks like this.



What happens?

---

\* e.g. by application of steady current

3) Amplitude-break excitation\*: From  $t = -\infty$  until  $t = 0$ , the transmembrane potential is clamped at some value  $v_*$  which is sufficiently negative that

$$n_{\infty}(v_*) < n_1$$

(Recall that  $n_1$  is the smallest value of  $n$  reached by the R branch of the slow manifold, see p. 13.)

At  $t = 0$ , the voltage clamp is removed. What happens?

Would the result be the same if a membrane at rest were suddenly stepped to the voltage  $v_*$ ? Explain the difference between these two situations. (Hint: think about  $n$ .)



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\* Use the un-shifted slow manifold (as shown on pp. 13-16) to answer this question.

Hodjkin-Huxley units.

voltage. mV

current:  $\mu A$

time: msec

length: cm

$\frac{\text{conductance}}{\text{area}}: \left( \frac{\mu A}{mV} \right) / \text{cm}^2$

$\frac{\text{capacitance}}{\text{area}}: \frac{(\mu A)(\text{msec})}{\text{mV} \cdot \text{cm}^2} = \mu F / \text{cm}^2$

/2

Hodgkin-Huxley parameters.

$$C = 1.0 \mu\text{F}/\text{cm}^2$$

$$\bar{I}_{Na} = 120 \left( \frac{\mu\text{A}}{\text{mV}} \right) / \text{cm}^2$$

$$\bar{I}_K = 36 \left( \frac{\mu\text{A}}{\text{mV}} \right) / \text{cm}^2$$

$$\bar{I}_L = 0.3 \left( \frac{\mu\text{A}}{\text{mV}} \right) / \text{cm}^2$$

$$E_{Na} = +45 \text{ mV}$$

$$E_K = -82 \text{ mV}$$

$$E_L = -59 \text{ mV}$$

$$a = 0.0238 \text{ cm}$$

$$\rho = 35.4 \Omega \text{ cm} = 0.0354 \left( \frac{\text{mV}}{\mu\text{A}} \right) \text{ cm}$$

## Hodgkin-Huxley functions

$$m_{\infty}(V) = \frac{\alpha_m(V)}{\alpha_m(V) + \beta_m(V)}$$

$$\tau_m(V) = \frac{1}{\alpha_m(V) + \beta_m(V)}$$

and similarly for  $n_{\infty}, \tau_n, h_{\infty}, \tau_h$

where the  $\alpha$ 's and  $\beta$ 's are given on the next page.

$$\alpha_m(V) = \frac{\left(\frac{V+45}{10}\right)}{1 - \exp\left(-\frac{V+45}{10}\right)}$$

$$\beta_m(V) = 4 \exp\left(-\frac{V+70}{18}\right)$$

$$\alpha_n(V) = (0.1) \frac{\left(\frac{V+60}{10}\right)}{1 - \exp\left(-\frac{V+60}{10}\right)}$$

$$\beta_n(V) = (0.125) \exp\left(-\frac{V+70}{80}\right)$$

$$\alpha_h(V) = (0.07) \exp\left(-\frac{V+70}{20}\right)$$

$$\beta_h(V) = \frac{1}{1 + \exp\left(-\frac{V+40}{10}\right)}$$

(V in mVolts,  $\alpha$  and  $\beta$  in  $\text{msec}^{-1}$ )

C. Peskin 10/22/91

1

## Singular-perturbation analysis of the Hodgkin-Huxley equations

We introduce a parameter  $\epsilon$  into the Hodgkin-Huxley equations as follows:

$$\begin{aligned} \epsilon C \frac{\partial v}{\partial t} + \bar{g}_{Na} m^3 h (v - E_{Na}) + \bar{g}_K n^4 (v - E_K) + \bar{g}_L (v - E_L) \\ = \epsilon^2 \frac{a}{2\tau} \frac{\partial^2 v}{\partial x^2} \end{aligned}$$

$$\epsilon \tau_m(v) \frac{\partial m}{\partial t} = m_\infty(v) - m$$

$$\tau_h(v) \frac{\partial h}{\partial t} = h_\infty(v) - h$$

$$\tau_n(v) \frac{\partial n}{\partial t} = n_\infty(v) - n$$

Note that  $\epsilon$  appears in 3 places: the  $\partial v / \partial t$  term, the  $\partial m / \partial t$  term, and the  $\partial^2 v / \partial x^2$  term (in which it appears as  $\epsilon^2$ ).

Clearly, we recover the original Hodgkin-Huxley equations by setting  $\epsilon = 1$ . We shall analyze the limit  $\epsilon \rightarrow 0$ . If the parameter  $\epsilon$  has been introduced cleverly enough, this limit will give a good approximation to the case  $\epsilon = 1$ .

To simplify matters, consider a special case. Let

$\tau_m$ ,  $\tau_h$ , and  $\tau_n$  be independent of  $v$

$$\tau_m = 0$$

$$m_\infty(v) = 1 - h_\infty(v) = n_\infty(v) = \begin{cases} 1 & v > v_* \\ 0 & v < v_* \end{cases}$$

where

$$E_K < E_L < v_* < 0 < E_{Na}$$

Since  $\tau_m = 0$ ,  $m = m_\infty(v)$ . Since  $m_\infty(v)$  is 0 or 1,  $m^3 = m$ .

Thus, we have the simplified system:

$$\epsilon C \frac{\partial v}{\partial t} + \bar{g}_{Na} m h (v - E_{Na}) + \bar{g}_K n^4 (v - E_K) + \bar{g}_L (v - E_L) = \epsilon^2 \frac{a}{2p} \frac{\partial^2 v}{\partial x^2}$$

$$m = \begin{cases} 1 & v > v_* \\ 0 & v < v_* \end{cases}$$

$$\tau_h \frac{\partial h}{\partial t} = (1 - m) - h$$

$$\tau_n \frac{\partial n}{\partial t} = m - n$$

(Note that  $v_*$  plays the role of an explicit threshold.)

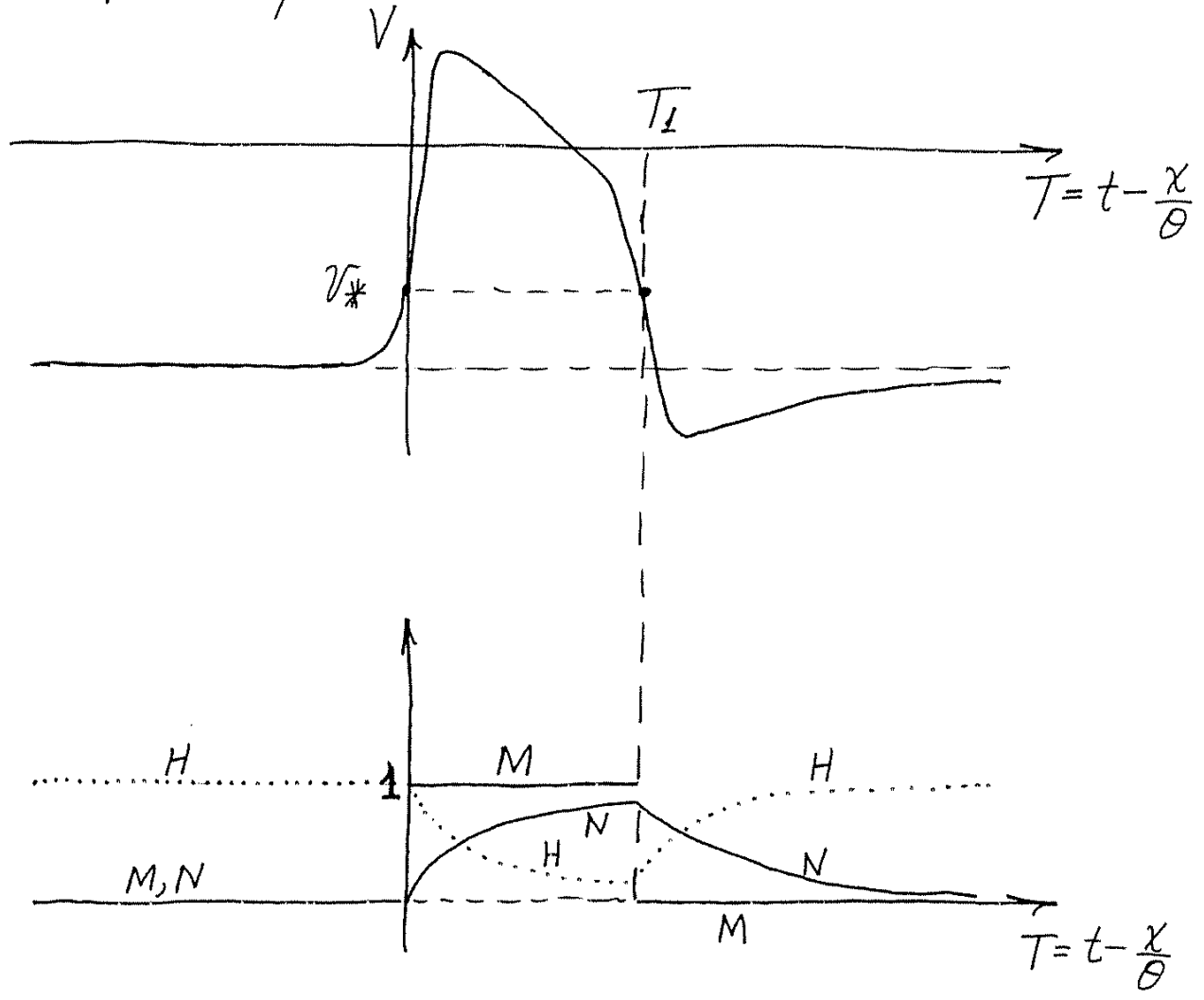


We seek traveling wave solutions:

$$v(x,t) = V\left(t - \frac{x}{\theta}\right) = V(T) \quad m(x,t) = M\left(t - \frac{x}{\theta}\right) = M(T)$$

$$h(x,t) = H\left(t - \frac{x}{\theta}\right) = H(T) \quad n(x,t) = N\left(t - \frac{x}{\theta}\right) = N(T)$$

with the following qualitative behavior:



For now, assume  $\theta$  and  $T_1$  are known. They will be determined later.

Solutions for M, H, N

$$M(T) = \begin{cases} 0, & T < 0 \\ 1, & 0 < T < T_1 \\ 0, & T_1 < T \end{cases}$$

$$H(T) = \begin{cases} 1, & T < 0 \\ \exp\left(-\frac{T}{\tau_h}\right), & 0 < T < T_1 \\ 1 - \left(1 - \exp\left(-\frac{T_1}{\tau_h}\right)\right) \exp\left(-\frac{T - T_1}{\tau_h}\right), & T_1 < T \end{cases}$$

$$N(T) = \begin{cases} 0, & T < 0 \\ 1 - \exp\left(-\frac{T}{\tau_n}\right), & 0 < T < T_1 \\ \left(1 - \exp\left(-\frac{T_1}{\tau_n}\right)\right) \exp\left(-\frac{T - T_1}{\tau_n}\right), & T_1 < T \end{cases}$$

Equation for V:

$$-\epsilon^2 \frac{a}{2\rho\theta^2} V''' + \epsilon C V'$$

$$+ \bar{g}_{Na} MH(V - E_{Na}) + \bar{g}_K N^4(V - E_K) + \bar{g}_L (V - E_L) = 0$$

"Outer solution" (valid away from  $T=0$  and  $T=T_1$ )  
 let  $\epsilon \rightarrow 0$  and solve for V:

$$V = \frac{\bar{g}_{Na} MH E_{Na} + \bar{g}_K N^4 E_K + \bar{g}_L E_L}{\bar{g}_{Na} MH + \bar{g}_K N^4 + \bar{g}_L}$$

where  $M, H, N$  are given on previous page. In particular

$$V = \begin{cases} E_L & T < 0 \\ \frac{\bar{g}_{Na} H E_{Na} + \bar{g}_K N^4 E_K + \bar{g}_L E_L}{\bar{g}_{Na} H + \bar{g}_K N^4 + \bar{g}_L}, & 0 < T < T_1 \\ \frac{\bar{g}_K N^4 E_K + \bar{g}_L E_L}{\bar{g}_K N^4 + \bar{g}_L}, & T_1 < T \end{cases}$$

"Inner solution" valid near  $T=0$ . Let  $T = \varepsilon S$

$$V(T) = V(\varepsilon S) = U(S)$$

$$\text{Then } U'(S) = \varepsilon V'(\varepsilon S) \quad U''(S) = \varepsilon^2 V''(\varepsilon S)$$

Substitute and then let  $\varepsilon \rightarrow 0$ .

$$-\frac{a}{2\rho\theta^2} U'' + C U' + \bar{g}_{Na} M H_0 (U - E_{Na}) + \bar{g}_K N_0^4 (U - E_K) + \bar{g}_L (U - E_L) = 0$$

$$\text{where } H_0 = \lim_{\varepsilon \rightarrow 0} H(\varepsilon S) = 1$$

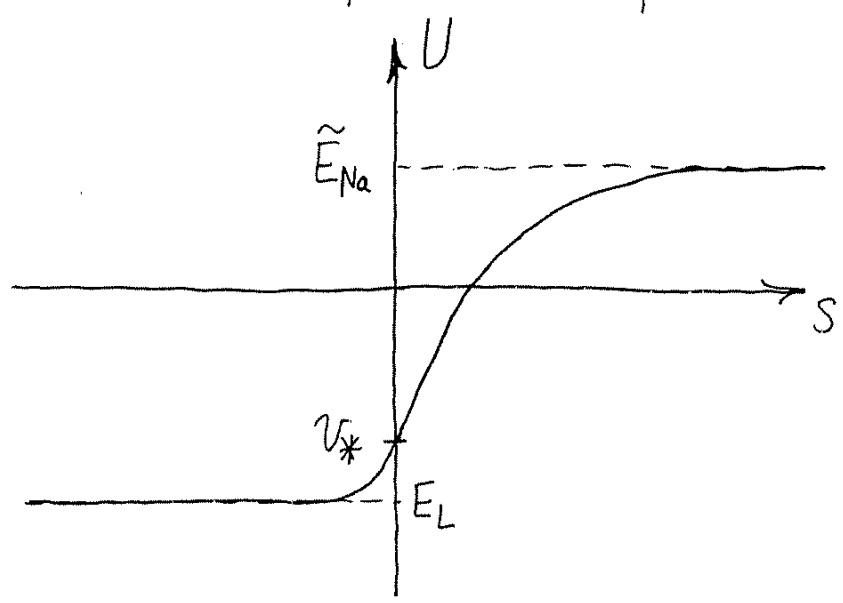
$$N_0 = \lim_{\varepsilon \rightarrow 0} N(\varepsilon S) = 0$$

$$M = \begin{cases} 1 & S > 0 \\ 0 & S < 0 \end{cases}$$

Hence

$$-\frac{a}{2\rho\theta^2} U'' + C U' + \bar{g}_{Na} M (U - E_{Na}) + \bar{g}_L (U - E_L) = 0$$

We seek a solution of the following form:



where

$$\tilde{E}_{Na} = \frac{\bar{g}_{Na} E_{Na} + \bar{g}_L E_L}{\bar{g}_{Na} + \bar{g}_L}$$

That is

$$U(s) = \begin{cases} E_L + (v_* - E_L) \exp(\lambda s) & s < 0 \\ \tilde{E}_{Na} + (v_* - \tilde{E}_{Na}) \exp(\mu s) & s > 0 \end{cases}$$

where  $\lambda$  is the positive root of

$$-\frac{a}{2\rho\theta^2} \lambda^2 + C\lambda + \bar{g}_L = 0$$

and  $\mu$  is the negative root of

$$-\frac{a}{2\rho\theta^2} \mu^2 + C\mu + (\bar{g}_{Na} + \bar{g}_L) = 0$$

It follows that

$$\lambda = \frac{\rho \theta^2 C}{a} \left( 1 + \sqrt{1 + \frac{2a \bar{g}_L}{\rho \theta^2 C^2}} \right)$$

$$\mu = \frac{\rho \theta^2 C}{a} \left( 1 - \sqrt{1 + \frac{2a(\bar{g}_L + \bar{g}_{Na})}{\rho \theta^2 C^2}} \right)$$

Note: The reason for choosing  $\lambda > 0$  and  $\mu < 0$  is to keep the solution bounded as  $S \rightarrow \mp \infty$ .

Because the equation for  $U$  is second-order, we require

$$U'(0^-) = U'(0^+)$$

$$(v_* - E_L) \lambda = (v_* - \tilde{E}_{Na}) \mu = (\tilde{E}_{Na} - v_*) (-\mu)$$

$$\frac{\lambda}{-\mu} = \frac{\tilde{E}_{Na} - v_*}{v_* - E_L} = r$$

$$\frac{\sqrt{1 + \frac{2a \bar{g}_L}{\rho \theta^2 C^2}} + 1}{\sqrt{1 + \frac{2a(\bar{g}_L + \bar{g}_{Na})}{\rho \theta^2 C^2}} - 1} = r$$

Solve for  $\theta$  as follows:

Let

$$A = \sqrt{1 + \frac{2a \bar{g}_L}{\rho \theta^2 C^2}}$$

$$B = \sqrt{1 + \frac{2a(\bar{g}_L + \bar{g}_{Na})}{\rho \theta^2 C^2}}$$

Then

$$\frac{A+1}{B-1} = r \quad \Rightarrow \quad A - rB = -r - 1$$

and

$$\frac{A^2 - 1}{B^2 - 1} = \frac{\bar{g}_L}{\bar{g}_L + \bar{g}_{Na}} = \alpha$$

$$\left(\frac{A-1}{B+1}\right)\left(\frac{A+1}{B-1}\right) = \alpha$$

$$\frac{A-1}{B+1} r = \alpha \quad \Rightarrow \quad rA - \alpha B = r + \alpha$$

$$A = \frac{\alpha r + \alpha + r^2 + \alpha r}{r^2 - \alpha} = \frac{r^2 + 2\alpha r + \alpha}{r^2 - \alpha}$$

$$B = \frac{r + \alpha + r^2 + r}{r^2 - \alpha} = \frac{r^2 + 2r + \alpha}{r^2 - \alpha}$$

Check:

$$A+1 = \frac{2r^2 + 2\alpha r}{r^2 - \alpha}$$

$$A-1 = \frac{2\alpha r + 2\alpha}{r^2 - \alpha}$$

$$B+1 = \frac{2r^2 + 2r}{r^2 - \alpha}$$

$$B-1 = \frac{2r + 2\alpha}{r^2 - \alpha}$$

$$\frac{A+1}{B-1} = \frac{2r(r+\alpha)}{2(r+\alpha)} = r \quad \checkmark$$

$$\frac{A-1}{B+1} = \frac{2\alpha(r+1)}{2r(r+1)} = \frac{\alpha}{r} \quad \checkmark$$

Now solve for  $\theta$  from  $A$  or  $B$ . For example

$$\theta^2 = \frac{2a(\bar{g}_L + \bar{g}_{Na})}{\rho C^2} \frac{1}{B^2 - 1}$$

$$= \frac{2a(\bar{g}_L + \bar{g}_{Na})}{\rho C^2} \frac{(r^2 - \alpha)^2}{2r(r+1)2(r+\alpha)}$$

$$= \frac{a(\bar{g}_L + \bar{g}_{Na})}{2\rho C^2} \frac{(r^2 - \alpha)^2}{r(r+1)(r+\alpha)}$$



Note: This formula for  $Q^2$  is only valid when  $r^2 > \alpha$ .

If  $r^2 \leq \alpha$ , there is no solution. To see this recall that

$$r = \frac{A+1}{B-1}$$

$$\frac{r}{\alpha} = \frac{B+1}{A-1}$$

$$\frac{r^2}{\alpha} = \frac{A+1}{A-1} \frac{B+1}{B-1} > 1 \quad (\text{since } A > 1 \text{ and } B > 1)$$

In summary, for  $r^2 > \alpha$

$$Q = \pm (r^2 - \alpha) \sqrt{\frac{a(\bar{g}_L + \bar{g}_{Na})}{2\rho G^2 r(r+1)(r+\alpha)}}$$

where

$$r = \frac{\tilde{E}_{Na} - v_*}{v_* - E_L}$$

"Inner solution" valid near  $T=T_1$ . Let  $T=T_1+\varepsilon S$

$$V(T) = V(T_1 + \varepsilon S) = U(S)$$

$$U'(S) = \varepsilon V'(T_1 + \varepsilon S) \quad U''(S) = \varepsilon^2 V''(T_1 + \varepsilon S)$$

Substitute and then let  $\varepsilon \rightarrow 0$ :

$$-\frac{a}{z\rho\theta^2} U'' + C U' + \bar{g}_{Na} M H_1 (U - E_{Na}) + \bar{g}_K N_1^4 (U - E_K) + \bar{g}_L (U - E_L) = 0$$

where

$$H_1 = \lim_{\varepsilon \rightarrow 0} H(T_1 + \varepsilon S) = \exp\left(-\frac{T_1}{\tau_h}\right)$$

$$N_1 = \lim_{\varepsilon \rightarrow 0} N(T_1 + \varepsilon S) = 1 - \exp\left(-\frac{T_1}{\tau_n}\right)$$

$$M = \begin{cases} 1, & S < 0 \\ 0, & S > 0 \end{cases}$$

let

$$g_1 = \bar{g}_K N_1^4 + \bar{g}_L$$

$$g_1^+ = \bar{g}_{Na} H_1 + \bar{g}_K N_1^4 + \bar{g}_L$$

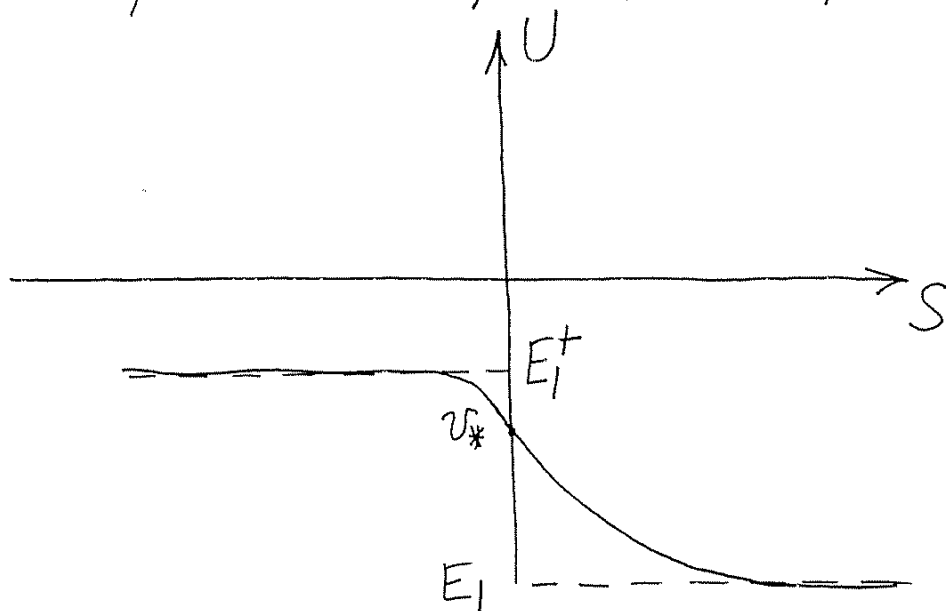
$$E_1 = \frac{\bar{g}_K N_1^4 E_K + \bar{g}_L E_L}{\bar{g}_K N_1^4 + \bar{g}_L}$$

$$E_1^+ = \frac{\bar{g}_{Na} H_1 E_{Na} + \bar{g}_K N_1^4 E_K + \bar{g}_L E_L}{\bar{g}_{Na} H_1 + \bar{g}_K N_1^4 + \bar{g}_L}$$

Then

$$-\frac{a}{2\rho\theta^2} U'' + CU' + \begin{cases} g_1^+(U-E_1^+) & S < 0 \\ g_1(U-E_1) & S > 0 \end{cases} = 0$$

Look for a solution of the following form



$$U(S) = \begin{cases} E_1^+ + (v_* - E_1^+) \exp(\lambda S) & S < 0 \\ E_1 + (v_* - E_1) \exp(\mu S) & S > 0 \end{cases}$$

where  $\lambda$  is the positive root of

$$-\frac{a}{2\rho\theta^2} \lambda^2 + C\lambda + g_1^+ = 0$$

and  $\mu$  is the negative root of

$$-\frac{a}{2\rho\theta^2} \mu^2 + C\mu + g_1 = 0$$

Thus

$$\lambda = \frac{\rho \theta^2 C}{a} \left( 1 + \sqrt{1 + \frac{2ag_1^+}{\rho \theta^2 C^2}} \right)$$

$$\mu = \frac{\rho \theta^2 C}{a} \left( 1 - \sqrt{1 + \frac{2ag_1}{\rho \theta^2 C^2}} \right)$$

Match slopes at  $S=0$ :

$$U'(0^-) = U'(0^+)$$

$$(v_* - E_1^+) \lambda = (v_* - E_1) \mu$$

$$\frac{\lambda}{-\mu} = \frac{v_* - E_1}{E_1^+ - v_*} = r_1 \quad (\text{This defines } r_1)$$

Then:

$$\frac{\sqrt{1 + \frac{2ag_1^+}{\rho \theta^2 C^2}} + 1}{\sqrt{1 + \frac{2ag_1}{\rho \theta^2 C^2}} - 1} = r_1$$

This equation determines  $T_1$  (see below)

How does  $r_1 = \frac{v_* - E_1}{E_1^+ - v_*}$  depend on  $T_1$  ?

It is easy to check that

i)  $E_1$  is decreasing

$$E_1(0) = E_L < v_*$$

Hence  $E_1(T_1) < v_*$  for all  $T_1$

ii)  $E_1^+$  is decreasing

$$E_1^+(0) = \tilde{E}_{Na} > v_*$$

$$E_1^+(\infty) = \frac{\bar{g}_K E_K + \bar{g}_L E_L}{\bar{g}_K + \bar{g}_L} < v_*$$

Hence there is some  $T_1^*$  for which

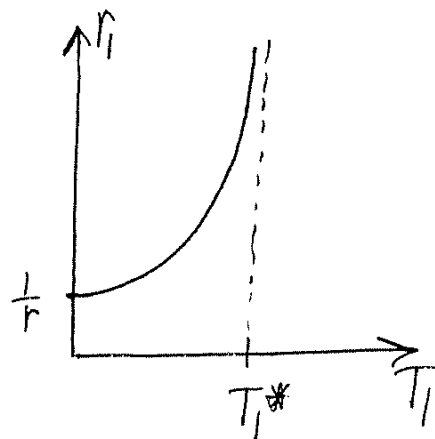
$$E_1^+(T_1^*) = v_*$$

It follows that:

$$r_1(0) = \frac{v_* - E_L}{\tilde{E}_{Na} - v_*} = \frac{1}{r}$$

$r_1$  is increasing

$r_1$  blows up at  $T_1 = T_1^*$



let

$$f_1(T_1) = \frac{\sqrt{1 + \frac{2a g_1^+(T_1)}{\rho \theta^2 C^2}} + 1}{\sqrt{1 + \frac{2a g_1(T_1)}{\rho \theta^2 C^2}} - 1}$$

First, note that

$$\begin{aligned} f_1(0) &= \frac{\sqrt{1 + \frac{2a(\bar{g}_{Na} + \bar{g}_L)}{\rho \theta^2 C^2}} + 1}{\sqrt{1 + \frac{2a \bar{g}_L}{\rho \theta^2 C^2}} - 1} \\ &> \frac{\sqrt{1 + \frac{2a(\bar{g}_{Na} + \bar{g}_L)}{\rho \theta^2 C^2}} - 1}{\sqrt{1 + \frac{2a \bar{g}_L}{\rho \theta^2 C^2}} + 1} = \frac{1}{r} = r_1(0) \end{aligned}$$

We have shown that  $f_1(0) > r_1(0)$

Next consider  $f_1'(T_1)$ . We have the following properties

$$g_1^+(T_1) > g_1(T_1) \quad (\text{because of } g_{Na})$$

$$(g_1^+)'(T_1) < g_1'(T_1) \quad (\text{because } g_{Na} \text{ is decreasing})$$

$$0 < g_1'(T_1) \quad (\text{because of } g_K)$$

It follows that  $f_1'(T_1) < 0$ . To show this, let

$$A_1 = \sqrt{1 + \frac{2a g_1^+(T_1)}{\rho \theta^2 C^2}}$$

$$B_1 = \sqrt{1 + \frac{2a g_1}{\rho \theta^2 C^2}}$$

$$f_1 = \frac{A_1 + 1}{B_1 - 1}$$

$$f_1' = \frac{(B_1 - 1)A_1' - (A_1 + 1)B_1'}{(B_1 - 1)^2}$$



Now

$$A_1' = \frac{a}{\rho \theta^2 c^2} \frac{1}{A_1} (g_1^+)'$$

$$B_1' = \frac{a}{\rho \theta^2 c^2} \frac{1}{B_1} g_1'$$

$$f_1' = \frac{a}{\rho \theta^2 c^2 (B_1 - 1)^2} \left[ \frac{(B_1 - 1)}{A_1} (g_1^+)' - \frac{(A_1 + 1)}{B_1} g_1' \right]$$

Now:

$$B_1 < A_1$$

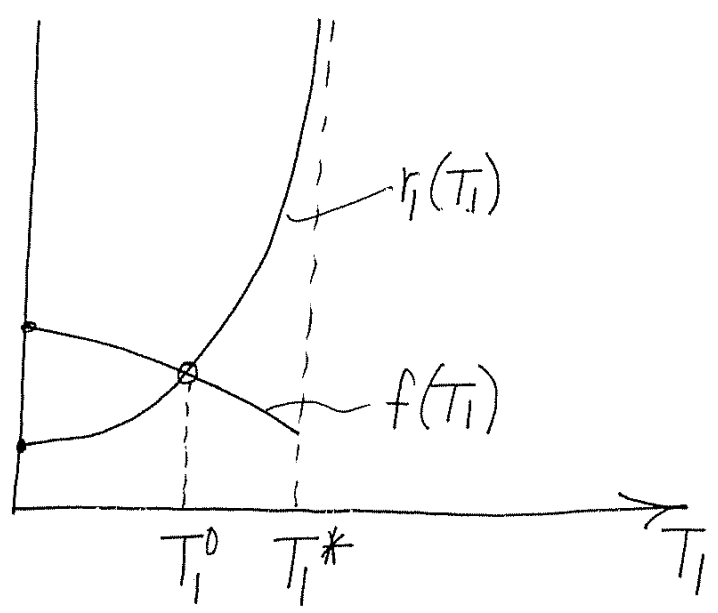
$$B_1 - 1 < A_1 + 1$$

$$\frac{B_1 - 1}{A_1} < \frac{A_1 + 1}{B_1}$$

$$\text{and } (g_1^+)' < g_1'$$

Hence  $f_1' < 0$  as claimed

We have shown that there is a unique  $T_1^0$  for which  $f_1(T_1^0) = r_1(T_1^0)$  :

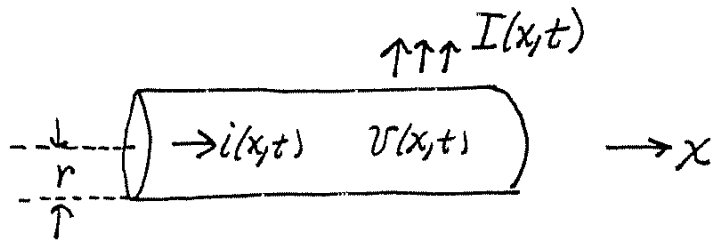


Thus  $T_1 = T_1^0$  is the duration of the pulse. Note that  $T_1^0 < T_1^*$ , the time at which the excited state would reach threshold. The pulse "jumps" across threshold on the downstroke just as on the upstroke. (It looks more and more like a jump as  $\epsilon \rightarrow 0$ .)

# NUMERICAL SOLUTION OF THE THE HODGKIN-HUXLEY EQUATIONS

C. Peskin 11/5/98

Derivation of the cable equation \*



$i(x,t)$  = axial current

$I(x,t)$  = transmembrane current (positive outward)

$v(x,t)$  = transmembrane voltage (inside - outside)

$r$  = radius of cable

Current conservation:

$$i(x_1, t) - i(x_2, t) = \int_{x_1}^{x_2} I(x, t) 2\pi r dx \quad (1)$$

$$0 = \int_{x_1}^{x_2} \left( \frac{\partial i}{\partial x} + I 2\pi r \right) dx \quad (2)$$

Since  $x_1$  and  $x_2$  are arbitrary

$$\frac{\partial i}{\partial x} + I 2\pi r = 0 \quad (3)$$

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\* First few pages here repeat earlier material, but are included to fix notation, which is slightly different.

Equation of transmembrane current:

$$I = C \frac{\partial v}{\partial t} + g(v - E) \quad (4)$$

Where  $C$  = capacitance per unit area of membrane  
 $g$  = conductance per unit area of membrane  
 $E$  = reversal potential (see below)

Equation of axial current

$$i = - \frac{\pi r^2}{\rho} \frac{\partial v}{\partial x} \quad (5)$$

Where  $\rho$  = resistivity of internal medium.

Substituting  $I$  and  $i$  into the equation of charge conservation. The result is

$$C \frac{\partial v}{\partial t} + g(v - E) = \frac{r}{2\rho} \frac{\partial^2 v}{\partial x^2} \quad (6)$$

Ionic current:

The ionic transmembrane current, denoted above as  $g(v-E)$  actually has three components that flow through different membrane channels:

$$g(v-E) = g_{Na}(v-E_{Na}) + g_K(v-E_K) + g_L(v-E_L) \quad (7)$$

The first two are caused by  $Na^+$  and  $K^+$  ions, respectively. The third type of ion channel is less specific and is denoted by the subscript L, for "Leakage." From Eq. 7, we have

$$g = g_{Na} + g_K + g_L \quad (8)$$

$$E = \frac{g_{Na} E_{Na} + g_K E_K + g_L E_L}{g_{Na} + g_K + g_L} \quad (9)$$

The quantities  $E_{Na}$ ,  $E_K$ , and  $E_L$  are constants. They are known as "equilibrium potentials" in the case of channels that admit only one species of ion like the  $Na^+$  and  $K^+$  channels. More generally, these constants are called "reversal potentials." They describe the voltage that must be applied to counterbalance the concentration difference of ions across the channels, and thus yield zero current.

In the case of a channel that admits only one species of ion, it can be shown from thermodynamic considerations that the equilibrium potential is given by the Nernst equation

$$E_{Na} = \frac{kT}{f} \log \frac{[Na^+]_o}{[Na^+]_i} \quad (10)$$

$$E_K = \frac{kT}{f} \log \frac{[K^+]_o}{[K^+]_i} \quad (11)$$

where

$k$  = Boltzmann's constant

$T$  = absolute temperature

$f$  = charge on a proton

$\log$  = natural logarithm

$[ ]_o$  = concentration outside cell

$[ ]_i$  = concentration inside cell

For less specific ion channels, the situation is more complicated, but one can still measure the voltage at which the current is zero, and that defines the reversal potential.

In typical neurons, the flow of current during an action potential is not sufficient to change the ion concentrations appreciably. Therefore, the quantities  $E_{Na}$ ,  $E_K$ , and  $E_L$  may be treated as constants. These constants satisfy

$$E_K < E_{rest} < E_L < 0 < E_{Na} \quad (12)$$

where  $E_{rest} = -70 \text{ mV}$  is the rest potential of the neuron.

Dynamics of the conductances:

The conductances  $g_{Na}$ ,  $g_K$ , and  $g_L$  obey the following equations:

$$g_{Na} = \bar{g}_{Na} m^3 h \quad (13)$$

$$g_K = \bar{g}_K n^4 \quad (14)$$

$$g_L = \bar{g}_L \quad (15)$$

where

$$\frac{\partial m}{\partial t} = \alpha_m(v)(1-m) - \beta_m(v)m \quad (16)$$

$$\frac{\partial h}{\partial t} = \alpha_h(v)(1-h) - \beta_h(v)h \quad (17)$$

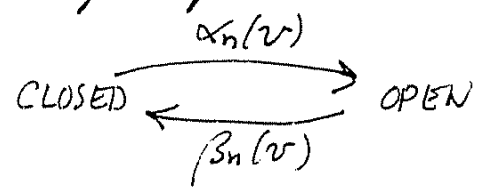
$$\frac{\partial n}{\partial t} = \alpha_n(v)(1-n) - \beta_n(v)n \quad (18)$$

where  $\bar{g}_{Na}$ ,  $\bar{g}_K$ ,  $\bar{g}_L$  are given constants, and where

$\alpha_m, \beta_m, \alpha_h, \beta_h, \alpha_n, \beta_n$  are given functions.

The following model of a  $K^+$  channel was proposed by Hodgkin and Huxley as a way of understanding Eqs. 14 and 18:

- i) Each  $K^+$  channel contains 4 identical gates
- ii) The gates open and close independently of each other
- iii) The rate constants for opening and closing a gate are voltage-dependent:



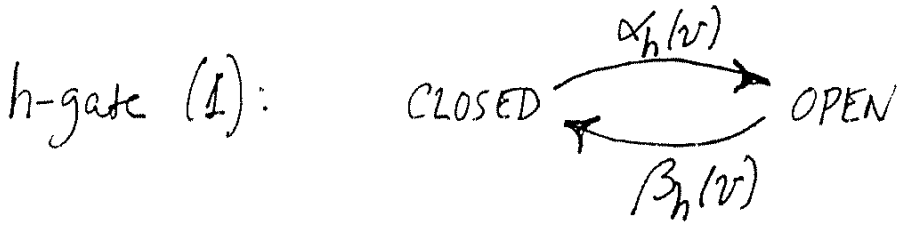
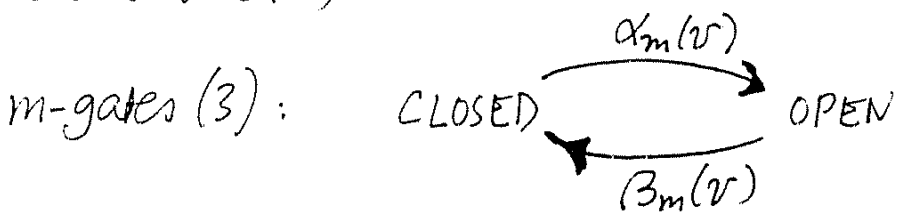
- iv) The  $K^+$  channel as a whole is open if and only if all four gates are open.

If we then let  $n$  = probability that a gate is open, and if we consider a large population of channels, Eqs. 14 and 18 follow.



Similarly, Eqs. 13,16,17, which describe the population of  $\text{Na}^+$  channels, can be understood in terms of the following model, proposed by Hodgkin and Huxley:

- i) Each  $\text{Na}^+$  channel contains 4 gates: 3 "m-gates" and 1 "h-gate."
- ii) All four gates open and close independently of each other.
- iii) The rate constants for opening and closing a gate are voltage dependent, with different voltage dependence for the m-gates and the h-gates. (Indeed, that is what distinguishes them from each other.)



- iv) The  $\text{Na}^+$  channel as a whole is open if and only if all four gates are open.

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If we then let

$m$  = probability that an  $m$ -gate is open  
 $h$  = probability that an  $h$ -gate is open

and consider a large population of channels,  
 Eqs. 13, 16, 17 follow.

Summary of the Hodgkin-Huxley equations:

$$C \frac{\partial V}{\partial t} + g(V-E) = \frac{r}{z_0} \frac{\partial^2 V}{\partial x^2} \quad (19)$$

$$g = g_{Na} + g_K + g_L \quad (20)$$

$$E = \frac{g_{Na} E_{Na} + g_K E_L + g_L E_L}{g_{Na} + g_K + g_L} \quad (21)$$

$$g_{Na} = \bar{g}_{Na} m^3 h \quad (22)$$

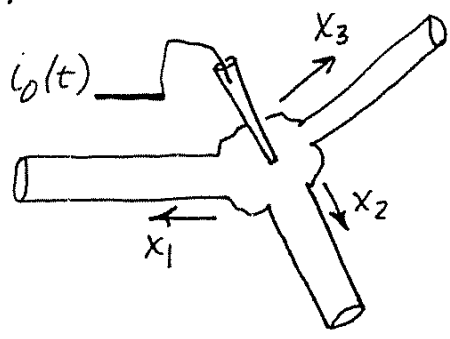
$$g_K = \bar{g}_K n^4 \quad (23)$$

$$g_L = \bar{g}_L \quad (24)$$

$$\frac{\partial s}{\partial t} = \alpha_s(v)(1-s) - \beta_s(v)s \quad (25)$$

where  $s = m, h, \text{ or } n$

Boundary conditions



$L=3$

Consider a junction at which  $L$  cables come together, numbered  $l=1 \dots L$ . There may be a cell body or other varicosity at the junction which we designate by the subscript 0; in particular its membrane area is  $A_0$ , and the current injected at the junction (if any) is denoted  $i_0(t)$ . This current could be an experimental stimulus, as shown above, or a synaptic current.

For simplicity of notation, we assume that  $x$  is measured away from the junction in all of the cables that meet there. Thus, the junction itself is given by  $x_1 = \dots = x_L = 0$ .

The boundary conditions are that the voltage is continuous and the currents add up:

$$v_0(t) = v_1(0,t) = v_2(0,t) = \dots = v_L(0,t) \quad (26)$$

$$i_0(t) = A_0 \left( C \frac{\partial v_0}{\partial t} + g_0(v_0 - E_0) \right) + \sum_{l=1}^L \left( -\frac{\pi r_l^2}{\rho} \right) \frac{\partial v_l}{\partial x_l}(0,t) \quad (27)$$

In Eq. 27,  $g_0$  and  $E_0$  are not constants. Instead, they are given by equations like Eqs. 20-25. Details of these equations may be different in different branches, and also different in the cell body (or other varicosity).

There are many special cases of the above boundary conditions that cover different situations of interest:

- i) If no current is applied,  $i_0(t) = 0$ .
- ii) If there is no cell body or varicosity at a junction,  $A_0 = 0$ .
- iii) At the terminal end of a branch,  $A_0 = 0$  and  $L = 1$ .
- iv) If current is applied in the interior of a branch, the point where it is applied can be regarded as a junction between two branches with identical properties. Thus  $L = 2$ ,  $r_1 = r_2$ ,  $A_0 = 0$ .

## Initial conditions

Initial data for the Hodgkin-Huxley equations are the values of  $v, m, h, n$  at  $t=0$ . That is, we need to specify

$$v(x, 0), m(x, 0), h(x, 0), n(x, 0)$$

In an important special case, the neuron is initially "at rest." This means that  $v(x, 0) = v_r$ , where  $v_r$  is a constant, the determination of which will be discussed below. The corresponding values of  $m, h, n$  are found by setting  $\partial m / \partial t = \partial h / \partial t = \partial n / \partial t = 0$  with  $v = v_r$ . The results may be summarized:

$$s_r = s_{\infty}(v_r) \quad (28)$$

where

$$s_{\infty}(v) = \frac{\alpha_s(v)}{\alpha_s(v) + \beta_s(v)} \quad (29)$$

and  $s = m, h, n$ . Then  $v_r$  itself is the solution of  $\partial v / \partial t = 0$ , or

$$v_r = E_r = \frac{\bar{g}_{Na} (m_{\infty}(v_r))^3 h_{\infty}(v_r) E_{Na} + \bar{g}_K (n_{\infty}(v_r))^4 E_K + \bar{g}_L E_L}{\bar{g}_{Na} (m_{\infty}(v_r))^3 h_{\infty}(v_r) + \bar{g}_K (n_{\infty}(v_r))^4 + \bar{g}_L}$$

Numerical method for the Hodgkin-Huxley equations

let

$$v_j^k = v(j\Delta x, k\Delta t) \tag{31}$$

$$s_j^{k+1/2} = s(j\Delta x, (k+1/2)\Delta t) \tag{32}$$

where  $s = m, h, n$ , and similarly for other variables related to  $m, h, n$ . Then let

$$\frac{s_j^{k+1/2} - s_j^{k-1/2}}{\Delta t} = \alpha_s(v_j^k) \left( 1 - \frac{s_j^{k+1/2} + s_j^{k-1/2}}{2} \right) - \beta_s(v_j^k) \left( \frac{s_j^{k+1/2} + s_j^{k-1/2}}{2} \right) \tag{33}$$

$$C \frac{v_j^{k+1} - v_j^k}{\Delta t} + g_j^{k+1/2} \left( \frac{v_j^{k+1} + v_j^k}{2} - E_j^{k+1/2} \right) = \frac{r}{z\rho} \left( D^+ D^- \frac{v^{k+1} + v^k}{2} \right)_j \tag{34}$$

where

$$(D^+\phi)_j = \frac{\phi_{j+1} - \phi_j}{\Delta x} \quad (35)$$

$$(D^-\phi)_j = \frac{\phi_j - \phi_{j-1}}{\Delta x} \quad (36)$$

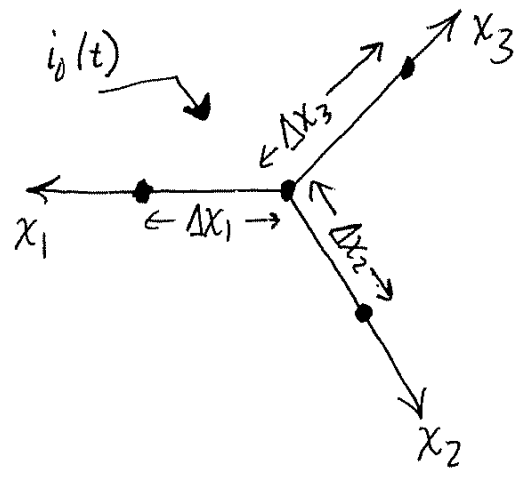
So that

$$(D^+D^-\phi)_j = (D^-D^+\phi)_j = \frac{\phi_{j+1} + \phi_{j-1} - 2\phi_j}{(\Delta x)^2} \quad (37)$$

Eqs. 33 are to be solved for  $s_j^{k+1/2}$ , and Eqs. 34 are to be solved for  $v_j^{k+1}$ .

Note that in Eqs. 33, the unknowns at different  $j$  are uncoupled, but in Eqs. 34 they are coupled through the operator  $D^+D^-$ . Thus Eq. 34 is a system to be solved simultaneously for all of the  $v_j$  at the particular time  $(k+1)\Delta t$ . This system is not completely specified, however, until we consider boundary conditions. (Eq. 34 only makes sense for interior points.)

Discretization of the boundary (junction) conditions



Since the voltage is continuous at a junction, we only need one node there. Let the junction voltage be denoted  $v_0(t)$ . This takes care of Eq. 26.

In order to discretize Eq. 27, we need a formula for  $\frac{\partial v_l}{\partial x_l}(0, t)$ . This is found from Taylor series:

$$v_l(\Delta x_l, t) = v_l(0, t) + \Delta x_l \frac{\partial v_l}{\partial x_l}(0, t) + \frac{1}{2}(\Delta x_l)^2 \frac{\partial^2 v_l}{\partial x_l^2}(0, t) + O((\Delta x_l)^3)$$

(38)



Note that the cable equation (Eq. 19) may be solved for  $\frac{\partial^2 V_l}{\partial x_l^2}$ :

$$\frac{\partial^2 V_l}{\partial x_l^2} = \frac{z_l}{r_l} \left( c \frac{\partial V_l}{\partial t} + g_l (V_l - E_l) \right) \quad (39)$$

Substitute Eq. 39 into Eq. 38, and solve for  $\frac{\partial V_l}{\partial x_l}(0,t)$ .

$$\begin{aligned} \frac{\partial V_l}{\partial x_l}(0,t) &= \frac{V_{l1} - V_0}{\Delta x_l} - \frac{2\Delta x_l \rho}{2r_l} \left( c \frac{\partial V_0}{\partial t} + g_{l0} (V_0 - E_{l0}) \right) \\ &\quad + O((\Delta x_l)^2) \end{aligned} \quad (40)$$

Substitute this result into Eq. 27 and collect terms:

$$\begin{aligned} i_0(t) &= \tilde{A}_0 \left( c \frac{\partial V_0}{\partial t} + \tilde{g}_0 (V_0 - \tilde{E}_0) \right) \\ &\quad + \sum_{l=1}^L \left( -\frac{\pi r_l^2}{\rho} \right) \frac{V_{l1} - V_0}{\Delta x_l} \\ &\quad + O((\Delta x)^2) \end{aligned} \quad (41)$$

where

$$\tilde{A}_0 = A_0 + \sum_{l=1}^L \frac{1}{2} (2\pi r_l \Delta x_l)$$

$$\tilde{g}_0 = \frac{A_0 g_0 + \sum_{l=1}^L \frac{1}{2} (2\pi r_l \Delta x_l) g_{l0}}{\tilde{A}_0}$$

$$\tilde{E}_0 = \frac{A_0 g_0 E_0 + \sum_{l=1}^L \frac{1}{2} (2\pi r_l \Delta x_l) g_{l0} E_{l0}}{\tilde{A}_0 \tilde{g}_0}$$

and where we have assumed that all the  $\Delta x_l$  are the same order of magnitude, denoted  $O(\Delta x)$ .

Our boundary or junction condition will be Eq. 41 with the  $O((\Delta x)^2)$  term deleted, and also discretized with respect to time:

$$i_0^{k+1/2} = \tilde{A}_0 \left( \left( \frac{v_0^{k+1} - v_0^k}{\Delta t} + \tilde{g}_0^{k+1/2} \left( \frac{v_0^{k+1} + v_0^k}{2} - E_0^{k+1/2} \right) \right) \right. \\ \left. + \sum_{l=1}^L \left( -\frac{\pi r_l^2}{\rho} \right) \frac{\left( \frac{v_{l1}^{k+1} + v_{l1}^k}{2} \right) - \left( \frac{v_0^{k+1} + v_0^k}{2} \right)}{\Delta x_l} \right) \quad (42)$$

Like the interior equations, this couples the junction point to its immediate neighbors only.

Next, we consider the solution of the resulting system of equations for  $v^{k+1}$ .

### Generalized tridiagonal system on a tree of nodes

Consider an arbitrary connected graph  $G$  with no loops.

Let the nodes of  $G$  be numbered  $1 \dots N$ , and let node 1 be called the root. (This can be any node of the graph; we choose it arbitrarily.)

Now consider some specified node  $i$ , where  $i \neq 1$ . Since  $G$  is connected, it is possible to find a chain of nodes connecting node 1 and node  $i$ . This is a sequence of node indices

$$(1, n_1, n_2, \dots, i)$$

such that the first element is 1, the last is  $i$ , there are no repetitions, and any two successive nodes in the chain are neighbors in  $G$ .

Since  $G$  has no loops, the chain of nodes connecting node 1 and node  $i$  is unique.

Let  $R(i)$  be the node that <sup>immediately</sup> precedes  $i$  in this chain. Then  $R(i)$  is the "rootward neighbor" of node  $i$ . This defines  $R(i)$  for all  $i \neq 1$ . By convention, we say that  $R(1) = 0$ .

Let  $L(i)$  be the set of all neighboring nodes of node  $i$  except  $R(i)$ . These will be

called the "leafward" neighbors of node  $i$ . A node  $i$  is said to be a "leaf" if it has no leafward neighbors; that is, if  $L(i) = \phi$ .

Thus, by choosing a root, we have made the graph  $G$  into a tree. This was only possible, of course, because  $G$  has no loops.

Now a generalized tridiagonal system on the tree defined above is a linear system of equations of the form

$$-a_i V_{R(i)} + b_i V_i - \sum_{j \in L(i)} c_{ij} V_j = W_j$$

$$i = 1 \dots N$$

(43)

where  $a_1 = 0$  and where the summation is understood to yield 0 when  $L(i) = \phi$ .

An important simplification of the notation can be made by noting that

$$j \in \mathcal{L}(i) \iff i = R(j) \quad (44)$$

Thus, for  $j \in \mathcal{L}(i)$

$$\bar{c}_{ij} = \bar{c}_{R(j),j} \quad (45)$$

which is a function of  $j$  only. Thus we may write

$$\bar{c}_{ij} = c_j \quad (46)$$

and our linear system becomes

$$-a_i V_{R(i)} + b_i V_i - \sum_{j \in \mathcal{L}(i)} c_j V_j = W_j \quad (47)$$

for  $i=1 \dots N$ . This system is solved by reducing it to a pair of generalized bidiagonal systems:

2)

$$b_i' U_i - \sum_{j \in \mathcal{I}(i)} c_j' U_j = W_i \quad (48)$$

$$-a_i' V_{R(i)} + V_i = U_i \quad (49)$$

Where the  $a_i'$ ,  $b_i'$ , and  $c_j'$  are to be determined  
So that Eqs. 48-49 are equivalent to Eq. 47.

To find out how these new coefficients are related to  
the original  $a_j$ ,  $b_i$ ,  $c_j$ , we substitute  
Eq. 49 into Eq. 48, and collect terms

$$b_i' (-a_i' V_{R(i)} + V_i) - \sum_{j \in \mathcal{I}(i)} c_j' (-a_j' V_{R(j)} + V_j) = W_i \quad (50)$$

$$\begin{aligned} & -b_i' a_i' V_{R(i)} + \left( b_i' + \sum_{j \in \mathcal{I}(i)} c_j' a_j' \right) V_i \\ & + \sum_{j \in \mathcal{I}(i)} (-c_j' V_j) = W_i \quad (51) \end{aligned}$$

The crucial step in the foregoing was to notice that for  $j \in \mathcal{L}(i)$ ,  $R(j) = i$ .

It is interesting to note that if instead of Eqs. 48-49, we had tried

$$-\tilde{a}'_i \tilde{U}_{R(i)} + \tilde{b}'_i \tilde{U}_i = W_i \quad (52)$$

$$\tilde{V}_i - \sum_{j \in \mathcal{L}(i)} \tilde{c}'_j \tilde{V}_j = \tilde{U}_i \quad (53)$$

we would not have been able to proceed. The reason can be seen when we substitute Eq. 53 into Eq. 52, to get

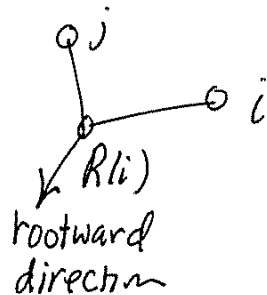
$$-\tilde{a}'_i \left( \tilde{V}_{R(i)} - \sum_{j \in \mathcal{L}(R(i))} \tilde{c}'_j \tilde{V}_j \right) + \tilde{b}'_i \left( \tilde{V}_i - \sum_{j \in \mathcal{L}(i)} \tilde{c}'_j \tilde{V}_j \right) = W_i \quad (54)$$



Eq. 54 is a dead end because

$$j \in \mathcal{L}(R(i)) \not\Rightarrow j=i \quad (55)$$

as shown by the following counterexample



Returning now to Eq. 51, and comparing it to Eq. 47, we see that the two are indeed of the same form and moreover that they can be made identical if we can choose  $a_i'$ ,  $b_i'$ , and  $c_j'$  to satisfy

$$a_i' b_i' = a_i \quad (56)$$

$$b_i' + \sum_{j \in \mathcal{L}(i)} c_j' a_j' = b_i \quad (57)$$

$$c_j' = c_j \quad (58)$$

Of course, Eq. 58 is easily satisfied merely by dropping the primes on the  $c_j$ ' and using instead the original coefficients  $c_j$ .

An algorithm will be stated below to find the  $a_i'$  and  $b_i'$  given the  $a_i$  and  $b_i$ . This algorithm depends on the nodes of the graph  $\mathcal{G}$  being numbered in such a manner that

$$j \in \mathcal{L}(i) \Rightarrow j > i \quad (59)$$

Such a numbering (of which there are many) can be found by induction. Start by assigning the number 1 to the root. Then, when the numbers  $1 \dots n$  have already been assigned, assign the number  $n+1$  to any node that does not yet have a number and which is connected by an edge of  $\mathcal{G}$  to some node that has already been numbered. Clearly, such a node exists since  $\mathcal{G}$  is connected, unless of course,  $n=N$  in which case we are done. Moreover, this procedure guarantees that

$$R(i) < i \quad (60)$$

for all  $i$ . To see this, recall the definition of  $R(i)$  as the node that immediately precedes  $i$  in the unique chain from the root to  $i$ . If

$i$  were numbered before  $R(i)$ , this would mean that there is some other chain from the root to  $i$ , one that does not involve  $R(i)$ . This is impossible, by the hypothesis that  $\mathcal{L}$  has no loops.

But

$$j \in \mathcal{L}(i) \Rightarrow R(j) = i \Rightarrow j > R(j) = i \Rightarrow j > i \quad (61)$$

where the second implication makes use of Eq. 60. Thus, we have proved Eq. 59. From now on, we assume that the nodes have been numbered in such a manner that Eq. 59 is satisfied.

Then the following algorithm finds the  $a_i'$  and  $b_i'$ , and moreover, it uses them to determine the  $U_i$  and finally the  $V_i$ :

for  $i = N : (-1) : 1$

$$b_i' = b_i - \sum_{j \in L(i)} c_j a_j'$$

$$a_i' = a_i / b_i'$$

$$U_i = (W_i + \sum_{j \in L(i)} c_j U_j) / b_i'$$

end

$$V_1 = U_1$$

for  $i = 2 : (+1) : N$

$$V_i = U_i + a_i' V_{R(i)}$$

end

Eqs. 59 and 60 guarantee that all quantities have already been computed by the time they are needed.

The efficient implementation of the above algorithm requires a good data structure for trees.

We shall call the nodes in the set  $\mathcal{L}(i)$  the "children" of node  $i$ .

Note that each node  $j$  other than the root ( $j=1$ ) is in exactly one of the sets  $\mathcal{L}(i)$ , namely  $\mathcal{L}(R(j))$ .

Let  $\mathcal{S}(j) = \mathcal{L}(R(j))$ . <sup>Eq. 62</sup> This is the set of "siblings" of node  $j$ . Also let

$$\mathcal{S}_+(j) = \{k : k \in \mathcal{S}(j) \text{ and } k > j\} \quad (63)$$

We shall think of this as the set of "younger siblings" of node  $j$ . Now let:

$$f_c(i) = \begin{cases} \text{Min}(\mathcal{L}(i)), & \mathcal{L}(i) \neq \phi \\ 0 & , \mathcal{L}(i) = \phi \end{cases} \quad (64)$$

$$ns(j) = \begin{cases} \text{Min}(\mathcal{S}_+(j)), & \mathcal{S}_+(j) \neq \phi \\ i & , \mathcal{S}_+(j) = \phi \end{cases} \quad (65)$$

Thus  $f_c(i)$  denotes the "first child" of node  $i$ , and  $ns(j)$  denotes the "next sibling" of node  $j$ . The entire tree can be reconstructed from these two arrays.

We now write a matlab program that uses the arrays  $fc$ ,  $ns$ , and  $R$  to implement the algorithm stated on page 26. This program stores  $a_i^j$  in the same location as  $a_i$ ,  $b_i^j$  in the same location as  $b_i$ , and  $U_i$  and  $W_i$  in the same location as  $V_i$ .

The main point of interest is the "while" loop that computes the sums over  $j \in \mathcal{L}(i)$ .

```

for i = N:(-1):1
    j = fc(i)
    while (j ~ = 0)
        b(i) = b(i) - c(j) * a(j)
        V(i) = V(i) + c(j) * V(j)
        j = ns(j)
    end
    a(i) = a(i) / b(i)
    V(i) = V(i) / b(i)
end
for j = 2:(+1):N
    V(i) = V(i) + a(i) * V(R(i))
end

```

Convergence of the proposed numerical method  
as applied to the cable equation on a periodic domain

In this section we consider the cable equation

$$C \frac{\partial v}{\partial t} + g(x,t)(v - E(x,t)) = \frac{r}{2\Delta} \frac{\partial^2 v}{\partial x^2} \quad (66)$$

on  $0 \leq x \leq L$  with periodic boundary conditions, and  $t > 0$ . The functions  $g(x,t)$  and  $E(x,t)$  are here regarded as known. This is, of course, a big simplification of the Hodgkin-Huxley case, in which  $g$  and  $E$  have to be determined by solving for  $m, h, n$ , which are themselves influenced by the voltage. The initial data are

$$v(x,0) = v^0(x), \text{ a given function} \quad (67)$$

The exact solution of the above problem,  $v(x,t)$ , also satisfies exactly the following difference scheme with remainder

$$\begin{aligned} C \frac{v^{n+1} - v^n}{\Delta t} + g^{n+1/2} \left( \frac{v^{n+1} + v^n}{2} - E^{n+1/2} \right) \\ = \frac{r}{2\Delta} D^+ D^- \frac{v^{n+1} + v^n}{2} + R^{n+1/2} \end{aligned} \quad (68)$$

Later, we shall use Taylor series to derive bounds on  $R^{n+1/2}$ , but for now we just regard it as some given function. Eq. 68 motivates the difference scheme

$$\begin{aligned} C \frac{V^{n+1} - V^n}{\Delta t} + g^{n+1/2} \left( \frac{V^{n+1} + V^n}{2} - E^{n+1/2} \right) \\ = \frac{r}{z\rho} D^+ D^- \frac{V^{n+1} + V^n}{2} \end{aligned} \quad (69)$$

let

$$U = V - v \quad (70)$$

so that  $U$  is the error. Subtracting Eq. 68 from Eq. 69, we see that  $U$  satisfies

$$\begin{aligned} C \frac{U^{n+1} - U^n}{\Delta t} + g^{n+1/2} \frac{U^{n+1} + U^n}{2} \\ = \frac{r}{z\rho} D^+ D^- \frac{U^{n+1} + U^n}{2} - R^{n+1/2} \end{aligned} \quad (71)$$

Also, if we set  $V^0 = v^0$ , then

$$U^0 = 0 \quad (72)$$



At this point we need the inner product defined by

$$(\phi, \psi) = \sum_{j=0}^{N-1} \phi_j \psi_j \Delta x \quad (73)$$

where  $\Delta x = L/N$ . Also, we shall use the corresponding norm

$$\|\phi\| = \sqrt{(\phi, \phi)} \quad (74)$$

Taking periodicity into account, it is easy to show by "summation by parts" (shifting indices) that

$$(\phi, D^+ \psi) = - (D^- \phi, \psi) \quad (75)$$

That is,  $D^+$  and  $(-D^-)$  are adjoint operators.

Applying this apparatus, we take the inner product of both sides of Eq. 71 with  $\frac{U^{n+1} + U^n}{2}$ . The result is

$$\begin{aligned}
& \frac{C}{2\Delta t} (\|U^{n+1}\|^2 - \|U^n\|^2) + \left( \frac{U^{n+1} + U^n}{2}, g^{n+1/2} \frac{U^{n+1} + U^n}{2} \right) \\
&= \frac{r}{2\tau} \left( \frac{U^{n+1} + U^n}{2}, D^+ D^- \frac{U^{n+1} + U^n}{2} \right) - \left( \frac{U^{n+1} + U^n}{2}, R^{n+1/2} \right)
\end{aligned} \tag{76}$$

Since  $g \geq 0$

$$\left( \frac{U^{n+1} + U^n}{2}, g \frac{U^{n+1} + U^n}{2} \right) \geq 0 \tag{77}$$

Also

$$\left( \frac{U^{n+1} + U^n}{2}, D^+ D^- \frac{U^{n+1} + U^n}{2} \right) = - \left\| D^- \frac{U^{n+1} + U^n}{2} \right\|^2 \leq 0 \tag{78}$$

Therefore, with the help of the Schwarz inequality

$$\frac{C}{2\Delta t} (\|U^{n+1}\|^2 - \|U^n\|^2) \leq \left\| \frac{U^{n+1} + U^n}{2} \right\| \left\| R^{n+1/2} \right\| \tag{79}$$

$$C \left( \frac{\|U^{n+1}\| + \|U^n\|}{2} \right) \left( \frac{\|U^{n+1}\| - \|U^n\|}{\Delta t} \right) \leq \left\| \frac{U^{n+1} + U^n}{2} \right\| \left\| R^{n+1/2} \right\| \tag{80}$$

By the triangle inequality

$$\left\| \frac{U^{n+1} + U^n}{2} \right\| \leq \frac{\|U^{n+1}\| + \|U^n\|}{2} \quad (81)$$

$$\Sigma \quad \|U^{n+1}\| - \|U^n\| \leq \frac{\Delta t}{C} \|R^{n+1/2}\| \quad (82)$$

Recall  $\|U^0\| = 0$ . It then follows by induction that for  $n\Delta t \leq t_{\max}$

$$\|U^n\| \leq \frac{t_{\max}}{C} \left( \max_{m: (m+1)\Delta t \leq t_0} \|R^{m+1/2}\| \right) \quad (83)$$

We now turn to the task of finding bounds on  $R$ .

This is done using Taylor series with remainder.

Let  $*$  denote the (unknown) time at which the remainder term is to be evaluated, and similarly, let  $*$  denote the (unknown) spatial location. Different instances of  $*$  or  $*$  may correspond to different values of  $t$  or  $x$ .

First, consider a Taylor series expansion in time about  $(j\Delta x, (n+\frac{1}{2})\Delta t)$

$$v_j^{n+1} = v_j^{n+1/2} + \left(\frac{\Delta t}{2}\right) \left(\frac{\partial v}{\partial t}\right)_j^{n+1/2} + \frac{1}{2} \left(\frac{\Delta t}{2}\right)^2 \left(\frac{\partial^2 v}{\partial t^2}\right)_j^{n+1/2} + \frac{1}{6} \left(\frac{\Delta t}{2}\right)^3 \left(\frac{\partial^3 v}{\partial t^3}\right)_j^{n+1/2} \quad (84)$$

$$v_j^n = v_j^{n+1/2} - \left(\frac{\Delta t}{2}\right) \left(\frac{\partial v}{\partial t}\right)_j^{n+1/2} + \frac{1}{2} \left(\frac{\Delta t}{2}\right)^2 \left(\frac{\partial^2 v}{\partial t^2}\right)_j^{n+1/2} - \frac{1}{6} \left(\frac{\Delta t}{2}\right)^3 \left(\frac{\partial^3 v}{\partial t^3}\right)_j^{n+1/2} \quad (85)$$

It follows that

$$\frac{v_j^{n+1} - v_j^n}{\Delta t} = \left(\frac{\partial v}{\partial t}\right)_j^{n+1/2} + \frac{(\Delta t)^2}{48} \left( \left(\frac{\partial^3 v}{\partial t^3}\right)_j^{n+1/2} + \left(\frac{\partial^3 v}{\partial t^3}\right)_j^{n+1/2} \right) \quad (86)$$

A similar argument shows that

$$\frac{v_j^{n+1} + v_j^n}{2} = v_j^{n+1/2} + \frac{(\Delta t)^2}{16} \left( \left(\frac{\partial^2 v}{\partial t^2}\right)_j^{n+1/2} + \left(\frac{\partial^2 v}{\partial t^2}\right)_j^{n+1/2} \right) \quad (87)$$

Next, considering a Taylor series expansion in space about the ~~same~~ point  $(j\Delta x, (n+\frac{1}{2})\Delta t)$ , we have

$$\begin{aligned}
 v_{j+1}^n &= v_j^n + (\Delta x) \left( \frac{\partial v}{\partial x} \right)_j^n + \frac{1}{2} (\Delta x)^2 \left( \frac{\partial^2 v}{\partial x^2} \right)_j^n \\
 &\quad + \frac{1}{6} (\Delta x)^3 \left( \frac{\partial^3 v}{\partial x^3} \right)_j^n + \frac{1}{24} (\Delta x)^4 \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n \quad (88)
 \end{aligned}$$

$$\begin{aligned}
 v_{j-1}^n &= v_j^n - (\Delta x) \left( \frac{\partial v}{\partial x} \right)_j^n + \frac{1}{2} (\Delta x)^2 \left( \frac{\partial^2 v}{\partial x^2} \right)_j^n \\
 &\quad - \frac{1}{6} (\Delta x)^3 \left( \frac{\partial^3 v}{\partial x^3} \right)_j^n + \frac{1}{24} (\Delta x)^4 \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n \quad (89)
 \end{aligned}$$

It follows that

$$\frac{v_{j+1}^n + v_{j-1}^n - 2v_j^n}{(\Delta x)^2} = \left( \frac{\partial^2 v}{\partial x^2} \right)_j^n + \frac{(\Delta x)^2}{24} \left( \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n \right) \quad (90)$$

Of course, Eq. 90 also holds with  $n$  replaced by  $n+1$ :

$$\frac{v_{j+1}^{n+1} + v_{j-1}^{n+1} - 2v_j^{n+1}}{(\Delta x)^2} = \left( \frac{\partial^2 v}{\partial x^2} \right)_j^{n+1} + \frac{(\Delta x)^2}{24} \left( \left( \frac{\partial^4 v}{\partial x^4} \right)_j^{n+1} + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^{n+1} \right) \quad (91)$$

Averaging Eq. 90 and Eq. 91, we get

$$\begin{aligned}
 & \left( D^+ D^- \frac{V^{n+1} + V^n}{2} \right)_j \\
 &= \frac{1}{2} \left( \left( \frac{\partial^2 V}{\partial x^2} \right)_j^{n+1} + \left( \frac{\partial^2 V}{\partial x^2} \right)_j^n \right) \\
 & \quad + \frac{(\Delta x)^2}{48} \left( \left( \frac{\partial^4 V}{\partial x^4} \right)_j^{n+1} + \left( \frac{\partial^4 V}{\partial x^4} \right)_j^{n+1} + \left( \frac{\partial^4 V}{\partial x^4} \right)_j^n + \left( \frac{\partial^4 V}{\partial x^4} \right)_j^n \right)
 \end{aligned}
 \tag{92}$$

Note that Eq. 87 applies not only to  $V$  but also to  $\partial^2 V / \partial x^2$ . In this form, it reads

$$\begin{aligned}
 & \frac{1}{2} \left( \left( \frac{\partial^2 V}{\partial x^2} \right)_j^{n+1} + \left( \frac{\partial^2 V}{\partial x^2} \right)_j^n \right) \\
 &= \left( \frac{\partial^2 V}{\partial x^2} \right)_j^{n+1/2} + \frac{(\Delta t)^2}{16} \left( \left( \frac{\partial^4 V}{\partial x^2 \partial t^2} \right)_j^* + \left( \frac{\partial^4 V}{\partial x^2 \partial t^2} \right)_j^* \right)
 \end{aligned}
 \tag{93}$$

Substituting Eq. 93 into Eq. 92, we get

$$\begin{aligned} (D^+ D^- \frac{v^{n+1} + v^n}{2})_j &= \left( \frac{\partial^2 v}{\partial x^2} \right)_j^{n+1/2} + \frac{(\Delta t)^2}{16} \left( \frac{\partial^4 v}{\partial x^2 \partial t^2} \right)_j^* + \left( \frac{\partial^4 v}{\partial x^2 \partial t^2} \right)_j^* \\ &+ \frac{(\Delta x)^2}{48} \left( \frac{\partial^4 v}{\partial x^4} \right)_j^{n+1} + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^{n+1} + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n \end{aligned} \quad (94)$$

Eq. 86 can be solved for  $(\partial v / \partial t)_j^{n+1/2}$ .

Eq. 87 can be solved for  $v_j^{n+1/2}$ .

Eq. 94 can be solved for  $(\partial^2 v / \partial x^2)_j^{n+1/2}$ .

Substituting these results into the cable equation, Eq. 66, we get Eq. 68 with

$$\begin{aligned} R_j^{n+1/2} &= C_1 \frac{(\Delta t)^2}{48} \left( \left( \frac{\partial^3 v}{\partial t^3} \right)_j^* + \left( \frac{\partial^3 v}{\partial t^3} \right)_j^* \right) \\ &+ g_i^{n+1/2} \frac{(\Delta t)^2}{16} \left( \left( \frac{\partial^2 v}{\partial t^2} \right)_j^* + \left( \frac{\partial^2 v}{\partial t^2} \right)_j^* \right) \\ &- \frac{r}{2\phi} \left[ \frac{(\Delta t)^2}{16} \left( \left( \frac{\partial^4 v}{\partial x^2 \partial t^2} \right)_j^* + \left( \frac{\partial^4 v}{\partial x^2 \partial t^2} \right)_j^* \right) \right. \\ &\left. + \frac{(\Delta x)^2}{48} \left( \left( \frac{\partial^4 v}{\partial x^4} \right)_j^{n+1} + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^{n+1} + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n + \left( \frac{\partial^4 v}{\partial x^4} \right)_j^n \right) \right] \quad (95) \end{aligned}$$

$$\text{Let } \|\phi\|_{\max} = \text{Max}_{\substack{0 \leq x \leq L \\ 0 \leq t \leq t_{\max}}} |\phi(x, t)| \quad (96)$$

Then, for  $0 \leq (n + \frac{1}{2})\Delta t \leq t_{\max}$ ,

$$|R_j^{n+1/2}| \leq A_1 (\Delta t)^2 + A_2 (\Delta x)^2 \quad (97)$$

where

$$A_1 = \frac{c}{24} \left\| \frac{\partial^3 v}{\partial t^3} \right\|_{\max} + \frac{\|g\|_{\max}}{8} \left\| \frac{\partial^2 v}{\partial t^2} \right\|_{\max} + \frac{r}{3\rho} \frac{1}{8} \left\| \frac{\partial^4 v}{\partial x^2 \partial t^2} \right\|_{\max} \quad (98)$$

$$A_2 = \frac{r}{3\rho} \frac{1}{12} \left\| \frac{\partial^4 v}{\partial x^4} \right\|_{\max} \quad (99)$$

Thus,  $A_1$  and  $A_2$  are constants, independent of  $\Delta t$  and  $\Delta x$



It follows from Eq. 97 that for  $0 \leq (n + \frac{1}{2})\Delta t \leq t_{max}$ ,

$$\|R^{n+1/2}\| \leq (A_1 (\Delta t)^2 + A_2 (\Delta x)^2) \sqrt{L} \quad (100)$$

Thus, finally, Eq. 83 becomes

$$\|V^n - v^n\| = \|U^n\| \leq \frac{t_{max} \sqrt{L}}{C} (A_1 (\Delta t)^2 + A_2 (\Delta x)^2) \quad (101)$$

where  $A_1$  and  $A_2$  are given by Eqs. 98-99.

Note that in the fixed time interval  $(0, t_{max})$ , we can make the error as small as we like by appropriate choice of  $\Delta t$  and  $\Delta x$ . This is called convergence of the numerical scheme.

Note that there is no restriction on  $\Delta t$  and  $\Delta x$ . This is called unconditional stability.

Finally, the error is  $O((\Delta t)^2) + O((\Delta x)^2)$ . This is called second-order accuracy.