Wrinkling of thin elastic sheets – Lecture 5: The floating elastic sheet

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Wrinkling – Lecture 4

Orientation

- Recall: *tension-induced* and *compressive* wrinkling are rather different. The annulus problem (Lecture 3) was tension-driven; the herringbone problem (Lecture 4) was compressive.
- Also recall the classic model problem

$$\min_{\substack{u=0 \text{ at } x=0\\ u_y=\pm 1}} \int u_x^2 + \varepsilon |u_{yy}|$$

where the *length scale* of the microstructure *depends on dist to bdry* (Lecture 2, and problem 3 of TA Session 2).

- Today's discussion concerns an example of tension-induced wrinkling that's analogous to that model problem.
- Joint work with Hoai-Minh Nguyen (preprint to come soon).

The floating elastic sheet

- sheet floats on water
- confined on 2 sides
- surface tension pulls free edges
- wrinkles form, refining at free edges





Experiment and some theory: Huang, Davidovitch, Santangelo, Russell, Menon (PRL 2010); also Davidovitch (PRE 2009)

Focus of today's discussion:

- Identify analogue of the relaxed problem and its solution.
- Estimate the energetic cost of changing the wrinkling length scale.

Heuristics

- sheet floats on water
- confined on 2 sides
- surface tension pulls free edges
- wrinkles form, refining at free edges





In the center: If length is large enough, end effects become irrelevant near center. Confinement requires wrinkling. Surface tension makes it tension-driven. Scale set by gravitational effects (prefers small amplitude) and bending (prefers few wrinkles).

At ends: Surface tension (miniscus effects) demand much smaller length scale.

Near ends: Refinement of wrinkling scale costs energy. A major goal of today's discussion: how to quantify this.

The energy

- Von Karman theory: displacement (w₁, w₂, u₃)
- Confinement: $w_2(x, 0) = 0, w_2(x, 1) = -\Delta/2$
- Domain $\Omega = [0, L] \times [0, 1]$, with $L \ge 1$
- For simplicity: *u*₃ is periodic in *y*



$$E_h = \alpha_m h \int_{\Omega} |\boldsymbol{e}(\boldsymbol{w}) + \frac{1}{2} \nabla u_3 \otimes \nabla u_3|^2 + h^3 \int_{\Omega} |\nabla \nabla u_3|^2 + \alpha_g \int_{\Omega} u_3^2 + \frac{1}{2} \alpha_s \int_{\Omega} |\nabla u_3|^2 - (\alpha_c - \alpha_s) \int_{\Omega} \partial_x w_1 + \alpha_c ||\boldsymbol{u}_3||^2_{H^{1/2}(\Gamma)}$$

Key hypothesis: $\alpha_c > \alpha_s$. Notation: Γ = free edges. Notes:

- Extra surf energy due to $u_3 \neq 0$ is $\alpha_s \int_{\Omega} \frac{1}{2} |\nabla u_3|^2 + \alpha_c ||u_3||^2_{H^{1/2}(\Gamma)}$
- Extra surf energy due to in-plane def is $(\alpha_s \alpha_c) \int_{\Omega} \text{div } w$
- Since $\int_{\Omega} \text{div } w = \int_{\Omega} \partial_x w_1 + \text{const, surf tension is tensile when } \alpha_c > \alpha_s.$
- $H^{1/2}$ term is energy of capillary fringe field:

$$\|u_3\|_{H^{1/2}(\Gamma)}^2 = \min \int_{\text{water}} |\nabla u_3|^2 = \sum_k |k| \left(|\hat{u}_3(0,k)|^2 + |\hat{u}_3(L,k)|^2 \right)$$

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Parameters, conventions, expectations

$$\begin{aligned} E_h &= \alpha_m h \int_{\Omega} |\boldsymbol{e}(\boldsymbol{w}) + \frac{1}{2} \nabla \boldsymbol{u}_3 \otimes \nabla \boldsymbol{u}_3|^2 + h^3 \int_{\Omega} |\nabla \nabla \boldsymbol{u}_3|^2 \\ &+ \alpha_g \int_{\Omega} \boldsymbol{u}_3^2 + \frac{1}{2} \alpha_s \int_{\Omega} |\nabla \boldsymbol{u}_3|^2 - (\alpha_c - \alpha_s) \int_{\Omega} \partial_x \boldsymbol{w}_1 + \alpha_c \|\boldsymbol{u}_3\|_{H^{1/2}(\Gamma)}^2 \end{aligned}$$

 α_m dimensionless

 α_g dimension: 1/length; gravitation, normalized by film stiffness

- α_s dimension: length; water-sheet surface energy, normalized
- α_c dimension: length; water-air surface energy, normalized
- *u*₃ mean 0, since water is incompressible

We expect

$$\min E_h = \begin{pmatrix} \text{value assoc} \\ \text{tensile effects} \end{pmatrix} + \begin{pmatrix} \text{correction due to presence} \\ \text{of bending energy} \end{pmatrix}.$$

First term is like "relaxed energy," second term is like "excess energy due to positive h," except that we haven't nondimensionalized.

A convenient reorganization

$$E_{h} = E_{1} + E_{2} + E_{3} + E_{4}$$

$$\begin{split} E_{1} &= \alpha_{m}h \int_{\Omega} (\partial_{x} w_{1} + \frac{1}{2} |\partial_{x} u_{3}|^{2})^{2} - (\alpha_{c} - \alpha_{s}) \int_{\Omega} (\partial_{x} w_{1} + \frac{1}{2} |\partial_{x} u_{3}|^{2}) \\ E_{2} &= \alpha_{m}h \int_{\Omega} (\partial_{y} w_{2} + \frac{1}{2} |\partial_{y} u_{3}|^{2})^{2} + \frac{1}{2} \alpha_{s} \int_{\Omega} |\partial_{y} u_{3}|^{2} \\ E_{3} &= h^{3} \int_{\Omega} |\nabla \nabla u_{3}|^{2} + \frac{1}{2} \alpha_{c} \int_{\Omega} |\partial_{x} u_{3}|^{2} + \alpha_{g} \int_{\Omega} u_{3}^{2} + \alpha_{c} ||u_{3}||_{H^{1/2}(\Gamma)}^{2} \\ E_{4} &= \frac{1}{2} \alpha_{m}h \int_{\Omega} |\partial_{x} w_{2} + \partial_{y} w_{1} + \partial_{x} u_{3} \partial_{y} u_{3}|^{2} \end{split}$$

- E_1 captures stretching due to surface tension. It slaves $\partial_1 w_1$ to $\partial_x u_3$.
- E_2 captures effect of confining bdry conditions. It determines $\int_0^1 (\partial_y u_3)^2$.
- Minimization of E₁ and E₂ gives the "value assoc to tensile forces."
- *E*₃ captures effect of bending resistance. Its min value is the "correction due to bending energy."
- E₄ is unimportant due to symmetry of bdry conditions.

Energy due to tensile forces

$$E_{1} = \alpha_{m}h \int_{\Omega} (\partial_{x}w_{1} + \frac{1}{2}|\partial_{x}u_{3}|^{2})^{2} - (\alpha_{c} - \alpha_{s}) \int_{\Omega} (\partial_{x}w_{1} + \frac{1}{2}|\partial_{x}u_{3}|^{2})$$
$$E_{2} = \alpha_{m}h \int_{\Omega} (\partial_{y}w_{2} + \frac{1}{2}|\partial_{y}u_{3}|^{2})^{2} + \frac{1}{2}\alpha_{s} \int_{\Omega} |\partial_{y}u_{3}|^{2}$$

- E_1 captures stretching due to surface tension. To minimize integrand, E_1 prefers $\partial_x w_1 + \frac{1}{2} |\partial_x u_3|^2$ to be a special value. So $\partial_x w_1$ is slaved to $\partial_x u_3$.
- *E*₂ captures effect of the confining bdry condition. Bdry condn gives $\int_0^1 \partial_y w_2 \, dy = -\Delta/2$. Claim: *E*₂ is minimized when, at each *x*, $z = \int_0^1 |\partial_y u_3|^2 \, dy$ achieves

$$\min_{z>0}\frac{\alpha_m h}{4}(\Delta-z)^2+\frac{1}{2}\alpha_s z.$$

• No wrinkling if best z is 0 (this occurs when $\alpha_m h\Delta < \alpha_s$).

Analysis of E_2

$$E_{2} = \alpha_{m}h\int_{\Omega}(\partial_{y}w_{2} + \frac{1}{2}|\partial_{y}u_{3}|^{2})^{2} + \frac{1}{2}\alpha_{s}\int_{\Omega}|\partial_{y}u_{3}|^{2}$$

For any x, let $z = z(x) = \int_0^1 (\partial_y u_3)^2 dy$. We have

$$\begin{aligned} -\frac{1}{2}\Delta + \frac{1}{2}z &= \int_{0}^{1} \partial_{y} w_{2} + \frac{1}{2} (\partial_{y} u_{3})^{2} dy \\ &\leq \left(\int_{0}^{1} |\partial_{y} w_{2} + \frac{1}{2} (\partial_{y} u_{3})^{2}|^{2} \right)^{1/2} \end{aligned}$$

Therefore

$$E_2 \geq \int_0^L \alpha_m h\left(\frac{z(x)-\Delta}{2}\right)^2 + \frac{1}{2}\alpha_s z(x)$$

$$\geq L\min_{z\geq 0}\left(\alpha_m h\left(\frac{z-\Delta}{2}\right)^2 + \frac{1}{2}\alpha_s z\right).$$

Moreover: if $\int_0^1 |\partial_y u_3|^2 dy$ deviates from the optimal value, E_2 will be larger (by an amount that's easy to determine).

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Summary thus far

The picture so far:

$$E_1 \ge -\frac{(\alpha_c - \alpha_s)^2}{4\alpha_m h}L, \quad E_2 \ge -\frac{1}{4}\alpha_m h\Delta^2 L - \frac{[\alpha_m h\Delta - \alpha_s]_+^2}{4\alpha_m h}L.$$

Equality holds in former when $\partial_x w_1 + \frac{1}{2} |\partial_x u_3|^2$ has the preferred value, so

 $\partial_x w_1$ is slaved to $\partial_x u_3$.

Equality holds in the latter when

$$\int_0^1 (\partial_y u_3)^2 \, dy = \delta \text{ for all } x,$$

with

$$\delta = \left[\frac{\alpha_m h \Delta - \alpha_s}{\alpha_m h}\right]_+$$

(which should be positive, to see wrinkling).

min E_1 + min E_2 is analogous to the min "relaxed energy" \mathcal{E}_0 of Lectures 2 & 3. If "excess energy" is small, then conditions noted above must be approx met.

Moving forward: E_3 controls the wrinkling. Recall:

$$E_3 = h^3 \int_{\Omega} \left| \nabla \nabla u_3 \right|^2 + \frac{1}{2} \alpha_c \int_{\Omega} \left| \partial_x u_3 \right|^2 + \alpha_g \int_{\Omega} u_3^2 + \alpha_c \|u_3\|_{H^{1/2}(\Gamma)}^2.$$

- The capillary term forces u_3 to be small at unconfined edges x = 0, L.
- If u₃ is uniformly small, then length scale of wrinkling must be small (since avg of |∂_yu₃|² was fixed by E₂). Expensive wrt bending energy.
- If u₃ is not uniformly small, then ∂_xu₃ must be large. Expensive wrt surface energy.

Evidently: length scale of wrinkling should vary with distance to edge. Focus for discussion: how does it vary, and what is the associated excess energy?

A heuristic argument

Arguing as for refinement of wrinkles in "annulus problem," we can construct $u_3(x, y)$ st $\int_0^1 (\partial_y u_3)^2 dy = \delta$ and there's a local length scale $\ell(x)$ for the wrinkling, with

$$|u_{3}| \sim \delta^{1/2} \ell(x), \quad |\partial_{x} u_{3}| \sim \delta^{1/2} \ell'(x) \quad |\nabla \nabla u_{3}| \sim \delta^{1/2} \ell^{-1}(x).$$

Since $E_{3} = h^{3} \int_{\Omega} |\nabla \nabla u_{3}|^{2} + \frac{1}{2} \alpha_{c} \int_{\Omega} |\partial_{x} u_{3}|^{2} + \alpha_{g} \int_{\Omega} u_{3}^{2} + \alpha_{c} ||u_{3}||^{2}_{H^{1/2}(\Gamma)}$ we get
 $E_{2} \sim h^{3} \int_{0}^{L} \delta \ell^{-2} dx + \frac{1}{2} \alpha_{c} \int_{0}^{L} \delta |\ell'|^{2} dx + \alpha_{c} \int_{0}^{L} \ell^{2} dx + \alpha_{c} \delta(\ell(0) + \ell(L))$

 $E_3 \sim \Pi \int_0^{\infty} \delta \ell \quad d\mathbf{x} + \frac{1}{2}\alpha_c \int_0^{\infty} \delta |\ell| \quad d\mathbf{x} + \alpha_g \int_0^{\infty} \ell \quad d\mathbf{x} + \alpha_c \delta(\ell(\mathbf{0}) + \ell(\mathbf{0})) + \delta(\ell(\mathbf{0})) + \delta(\ell($

Note: the final term is linear in ℓ since we expect

$$\int_0^1 |\partial_y^{1/2} u_3|^2 \, dy \sim \left(\int_0^1 u_3^2 \, dy\right)^{1/2} \left(\int_0^1 |\partial_y u_3|^2 \, dy\right)^{1/2}$$

Variation of the local length scale

Conclusion thus far: wrinkling length scale should minimize

$$\int_0^L \left(h^3 \ell^{-2} + \frac{1}{2}\alpha_c |\ell'|^2 + \alpha_g \ell^2\right) dx + \alpha_c(\ell(0) + \ell(L))$$

What to do with this?

(a) Study this 1D variational problem for $\ell(x)$.

(b) Draw qualitative conclusions, then seek ansatz-free results for E_3 . I'll focus on (b).

Easy warmup. If *L* is large enough, edge effects should be unimportant and ℓ should be indep of *x*. The assoc *bulk wrinkling scale* ℓ_B should achieve

$$\min_{\ell} h^3 \ell^{-2} + \alpha_g \ell^2$$

whence $\ell_B = (h^3 \alpha_g^{-1})^{1/4}$. We know the ansatz-free lower bound associated with this calculation: it uses the interpolation ineq

$$\int_0^1 |\partial_y u_3|^2 \, dy \le \left(\int_0^1 u_3^2 \, dy\right)^{1/2} \left(\int_0^1 |\partial_{yy} u_3|^2 \, dy\right)^{1/2}.$$

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The energetic cost of refinement

A different question: Suppose $\ell(0) \ll \ell_B$, and *L* is large enough that ℓ_B is achieved at x = L/2. What is the energetic cost of refinement?

In terms of ℓ the answer is easy:

$$\int_{0}^{L/2} h^{3} \ell^{-2} + \frac{1}{2} \alpha_{c} |\ell'|^{2} dx \geq \int_{0}^{L/2} \sqrt{2} h^{3/2} \alpha_{c}^{1/2} |\ell'/\ell| dx$$
$$\geq \sqrt{2} h^{3/2} \alpha_{c}^{1/2} \ln(\ell_{B}/\ell(0)).$$

Does this have an ansatz-free analogue? Yes! It is provided (after nondimensionalization) by

Proposition: If $g(x, y) : [0, 1]^2 \to \mathbb{R}$ is periodic in y and

•
$$\int_0^1 g^2(0, y) \, dy \le a$$
 (sufficiently small)

• $\int_0^1 g^2(1, y) dy \ge b$ (sufficiently large)

• $\int_0^1 (\partial_y g)^2(x, y) \, dy \ge 1$ for most x (all but measure ε)

then

$$t\int_0^1\int_0^1(\partial_{yy}g)^2+\alpha\int_0^1\int_0^1(\partial_xg)^2\geq C\sqrt{\alpha t}\log(b/a)$$

provided $\varepsilon \leq rac{lpha \sqrt{ab}}{2\sqrt{lpha t} \log(b/a)}$

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provided $\varepsilon \le \frac{\alpha \sqrt{ab}}{2\sqrt{\alpha t} \log(b/a)}$.

Proof of the proposition

Sketch of proof, assuming for simplicity that $\int_0^1 g^2(0, y) \, dy = a$, $\int_0^1 g^2(1, y) = b$, and $b = 4^n a$ for some *n*.

Step 1: Let x_j be the largest x st $\int_0^1 g^2(x, y) dy \ge 4^j a$. Note that $0 \le x_0 < x_1 < \cdots < x_n = 1$ and

$$\int_0^1 g^2(x,y)\,dy < 4^j a \quad \text{for } x > x_j;$$

also $\int_0^1 g^2(x_j, y) \, dy = 4^j a$, and (by triangle ineq)

$$\left(\int_0^1 |g(x_j, y) - g(x_{j+1}, y)|^2 \, dy\right)^{1/2} \ge \left(\int_0^1 g^2(x_{j+1}, y) \, dy\right)^{1/2} - \left(\int_0^1 g^2(x_j, y) \, dy\right)^{1/2}$$

Step 2: Observe that

$$\int_{\substack{x_j < x < x_{j+1} \\ 0 < y < 1}} (\partial_x g)^2 \, dx \, dy \geq \frac{1}{|x_{j+1} - x_j|} \int_0^1 |g(x_j, y) - g(x_{j+1}, y)|^2 \, dy$$

since LHS is minimized by the function that's affine in *x* with the same values at $x = x_j$ and x_{j+1} .

Proof of the proposition, cont'd

Step 3: Suppose now that $\int_0^1 g_y^2 dy \ge 1$ on at least half of (x_j, x_{j+1}) . Then our much-used interpolation ineq $(\int |\partial_y g|^2 dy)^2 \le \int g^2 dy \cdot \int |\partial_{yy} g|^2 dy$ gives

$$\int_{\substack{x_j < x < x_{j+1} \\ 0 < y < 1}} g_{yy}^2 \, dx \, dy \ge \frac{1}{4^j a} \frac{1}{2} |x_{j+1} - x_j|.$$

Combining this with outcome of step 2, we get

$$t \int_{\substack{x_j < x < x_{j+1} \\ 0 < y < 1}} g_{yy}^2 \, dx \, dy \quad + \quad \alpha \int_{\substack{x_j < x < x_{j+1} \\ 0 < y < 1}} g_x^2 \, dx \, dy$$
$$\geq \quad \frac{t}{4^j a} \cdot \frac{1}{2} |x_{j+1} - x_j| + \frac{\alpha}{|x_{j+1} - x_j|} \cdot 4^j a$$
$$\geq \quad C \sqrt{\alpha t}.$$

Repeating for each *j*, we get a total of order $\sqrt{\alpha t} \log(b/a)$ since $n \sim \log(b/a)$.

Proof of the proposition - cont'd

Step 4. We assumed in Step 3 that $\int_0^1 g_y^2 dy \ge 1$ on at least half of (x_j, x_{j+1}) . It's sufficient for Step 3 that this hold for at least half those intervals, eg for $j \ge n/2$.

Suppose Step 3 fails, because this condition fails for some $j \ge n/2$. Then

$$|x_j - x_{j+1}| \le C \varepsilon \le C rac{lpha \sqrt{ab}}{2\sqrt{lpha t} \log(b/a)}$$

and $4^j \ge (b/a)^{1/2}$. In this case

$$\begin{array}{lll} \alpha \int_{\substack{x_j < x < x_{j+1} \\ 0 < y < 1}} g_x^2 \, dx \, dy & \geq & \frac{\alpha}{|x_{j+1} - x_j|} 4^j a \\ & \geq & \frac{\alpha \sqrt{ab}}{|x_{j+1} - x_j|} \geq C \sqrt{\alpha t} \log(b/a) \end{array}$$

and the estimate is true anyway.







- Wrinkling can be microstructure (when its length scale \rightarrow 0 as $h \rightarrow$ 0).
- Advantage of focus on energy scaling law: permits ansatz-free analysis.
- Different tools have different strengths:
 - Numerics predicts patterns, but finds local minima
 - Minimization within an ansatz suggests what to expect
 - Ansatz-independent lower bounds confirm (or refute) adequacy of a particular ansatz
 - Lower bounds help explain *why* patterns form, and which features are most important

Stepping back - cont'd



• Some successes, but still many open problems.

- For the floating elastic sheet: is the local scale of wrinkling correctly predicted by our 1D var'l problem for $\ell(x)$?
- For the film bonded to a compliant substrate, are the labyrinth patterns comparable energetically to the herringbone pattern?
- For a "crumpled" piece of paper, does energy minimization require folds? How does the min energy scale with *h*?

• Wrinkling is just one example of energy-driven pattern formation

- Shape-memory materials, ferromagnets, liquid crystals, ...
- Energy min is a good guide in some systems, not in others.
- Many examples are "understood," through numerics or minimization within an ansatz.
- Attempts at rigorous analysis challenge our understanding.

Credits

Images are from:





J. Huang, B. Davidovitch, C. Santangelo, T. Russell, and N. Menon, *Phys Rev Lett* 105 (2010) 038302

J. Huang et al, *Science* 317 (2007) 650–653

X. Chen and J. Hutchinson, *Scripta Materialia* 50 (2004) 797–801



P.-C. Lin & S. Yang, Appl Phys Lett 90 (2007) 241903

S. Conti and F. Maggi, Arch Rational Mech Anal 187 (2008) 1-48